

Particle Impact Conditions and Corresponding Coating Properties in Cold Spraying

T. Schmidt, F. Gaertner, H. Kreye, T. Klassen

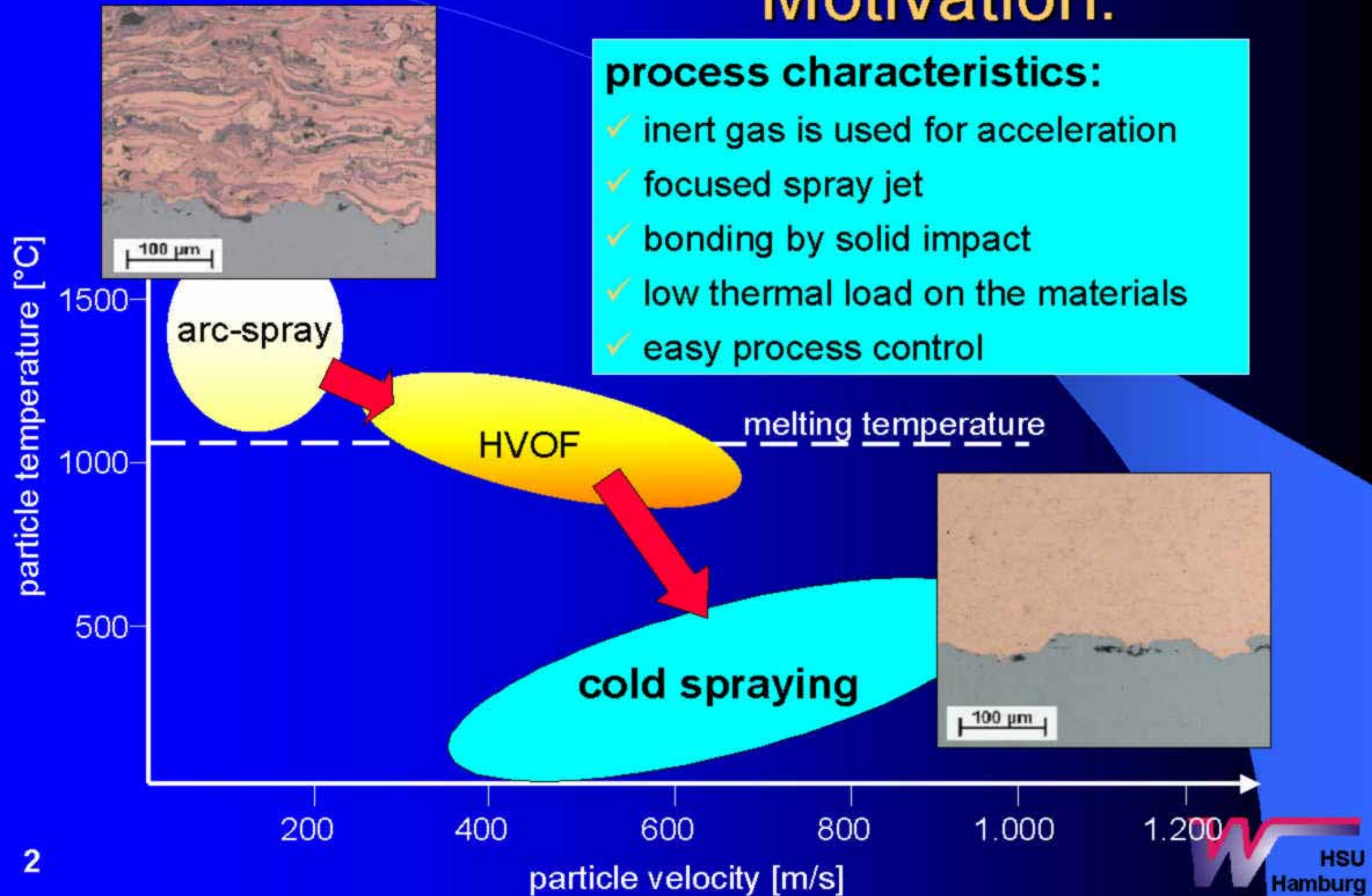
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Cold Spray 2007 Conference, October 8-9, Akron, Ohio, USA

Motivation:

process characteristics:

- ✓ inert gas is used for acceleration
- ✓ focused spray jet
- ✓ bonding by solid impact
- ✓ low thermal load on the materials
- ✓ easy process control



Outline

- particle bonding in cold spraying
- impact simulations showing the
 - ✓ effect of particle size on critical velocity
- optimisation strategy:
 - ✓ using an optimised size distribution
 - ✓ generating a distinct exceeding of V_{crit} by V_p
- realization of these conditions (new equipment)
- correlation of coating properties with impact conditions using the “**window of deposition**”

Particle Bonding in Cold Spray [2, 3]

- ✓ caused by a high strain rate deformation
- ✓ related to adiabatic shear instabilities
- ✓ requires sufficient high particle velocity $V_p > V_{crit}$



Particle Impact - FEM Modelling

software

- ABAQUS/Explicit

input

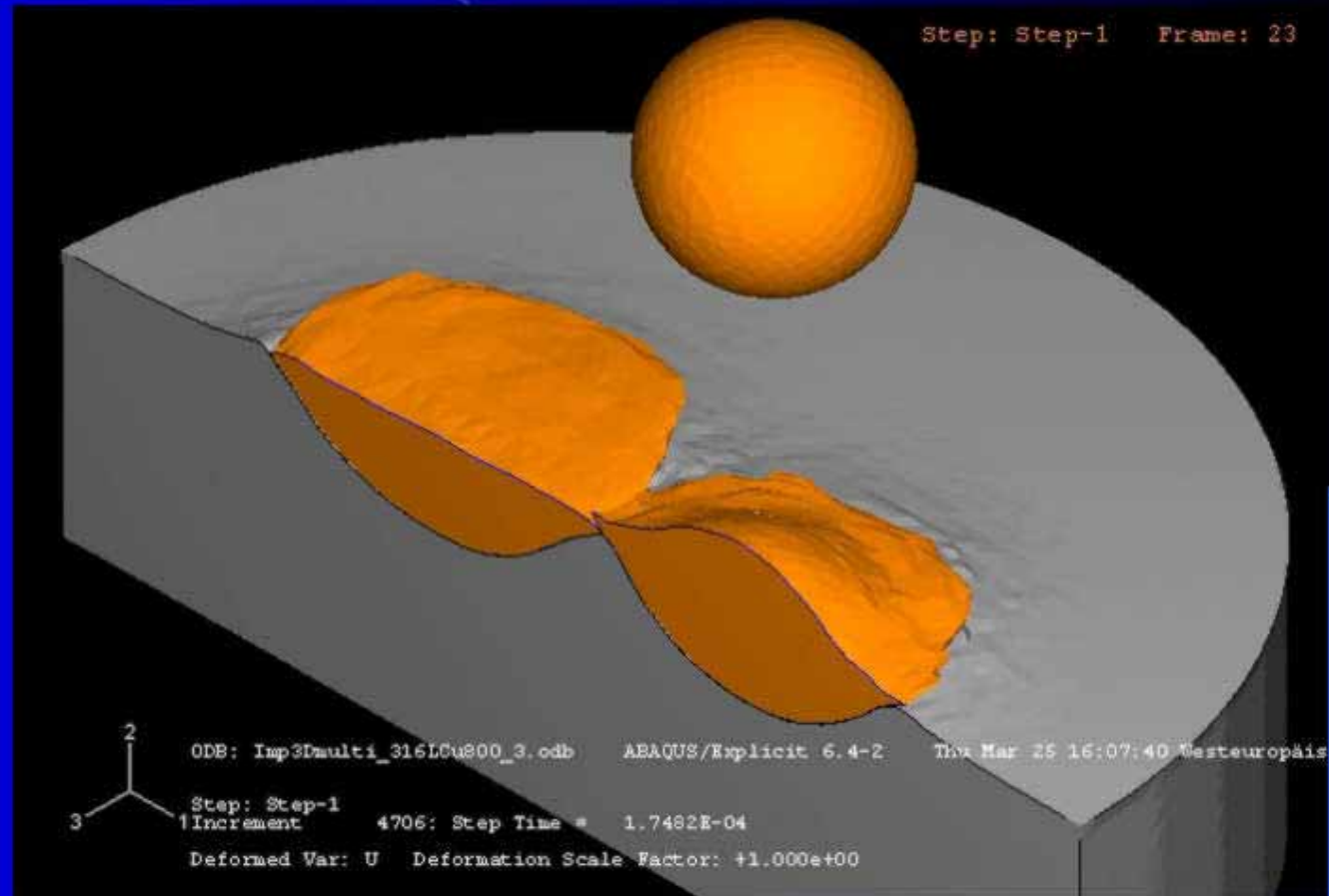
- material properties
- particle temperature
- particle velocity

output

- deformed shape
- field variables

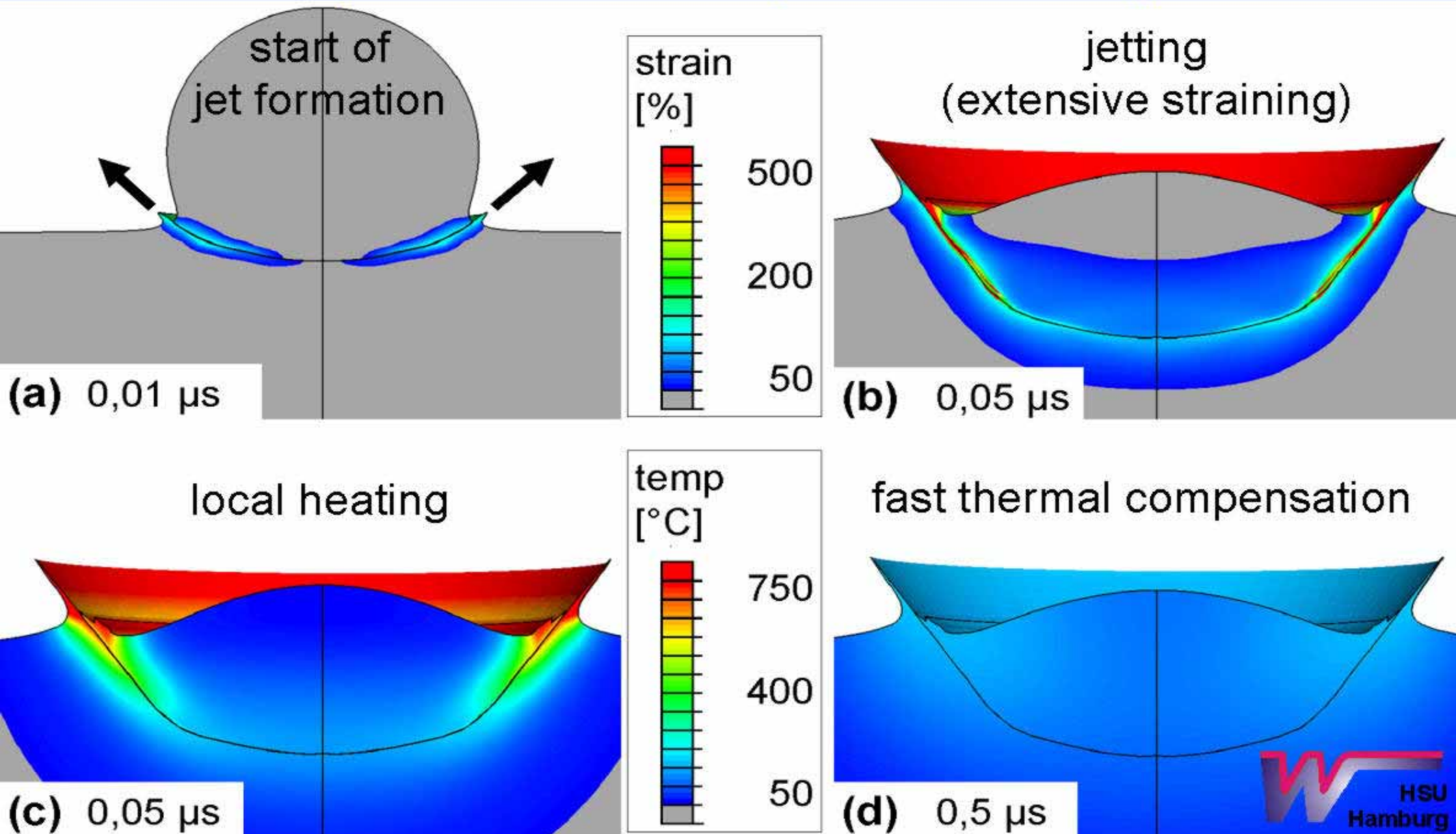
special

- thermally coupled analyse
- propagation of heat, generated by straining, is considered



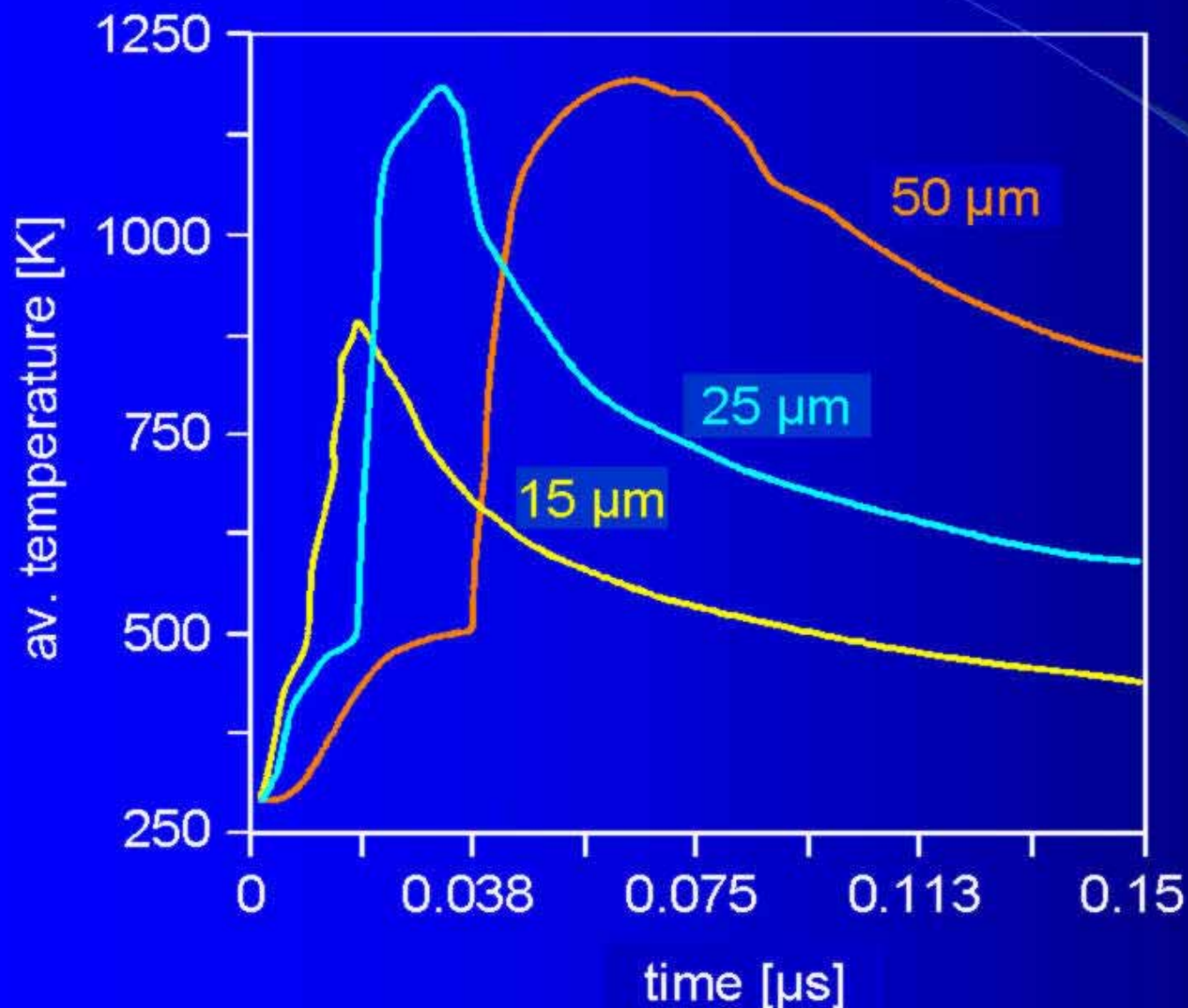
Particle Impact, Cu-Cu, 500 m/s, 20°C [3, 5]

cross-section particle - substrate, strain and temperature field



Effect of Particle Size

interface temperature Cu – Cu, 600 m/s, 20°C



temporal evolution of the interface temperature for different particle size at same conditions

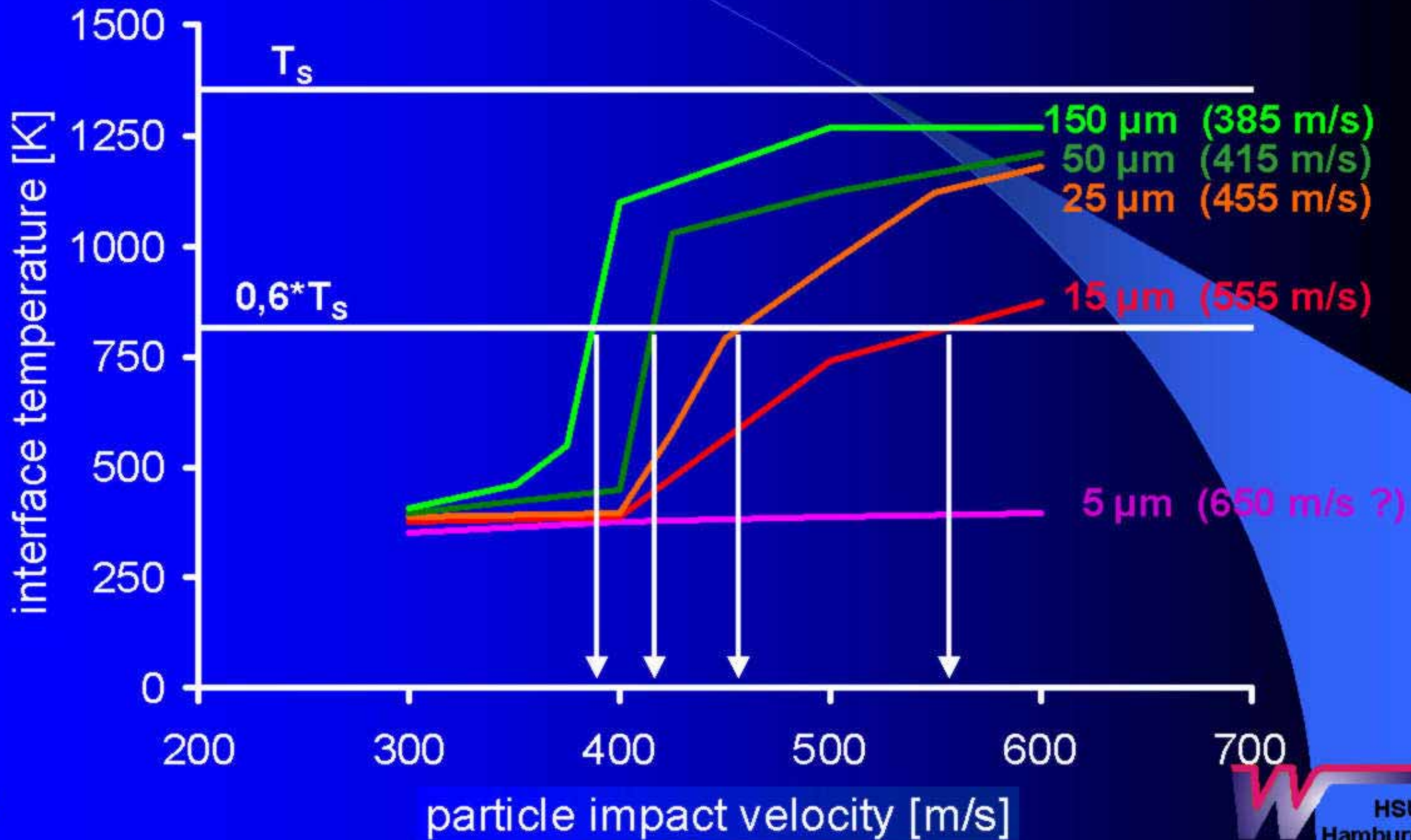


coarser particles:

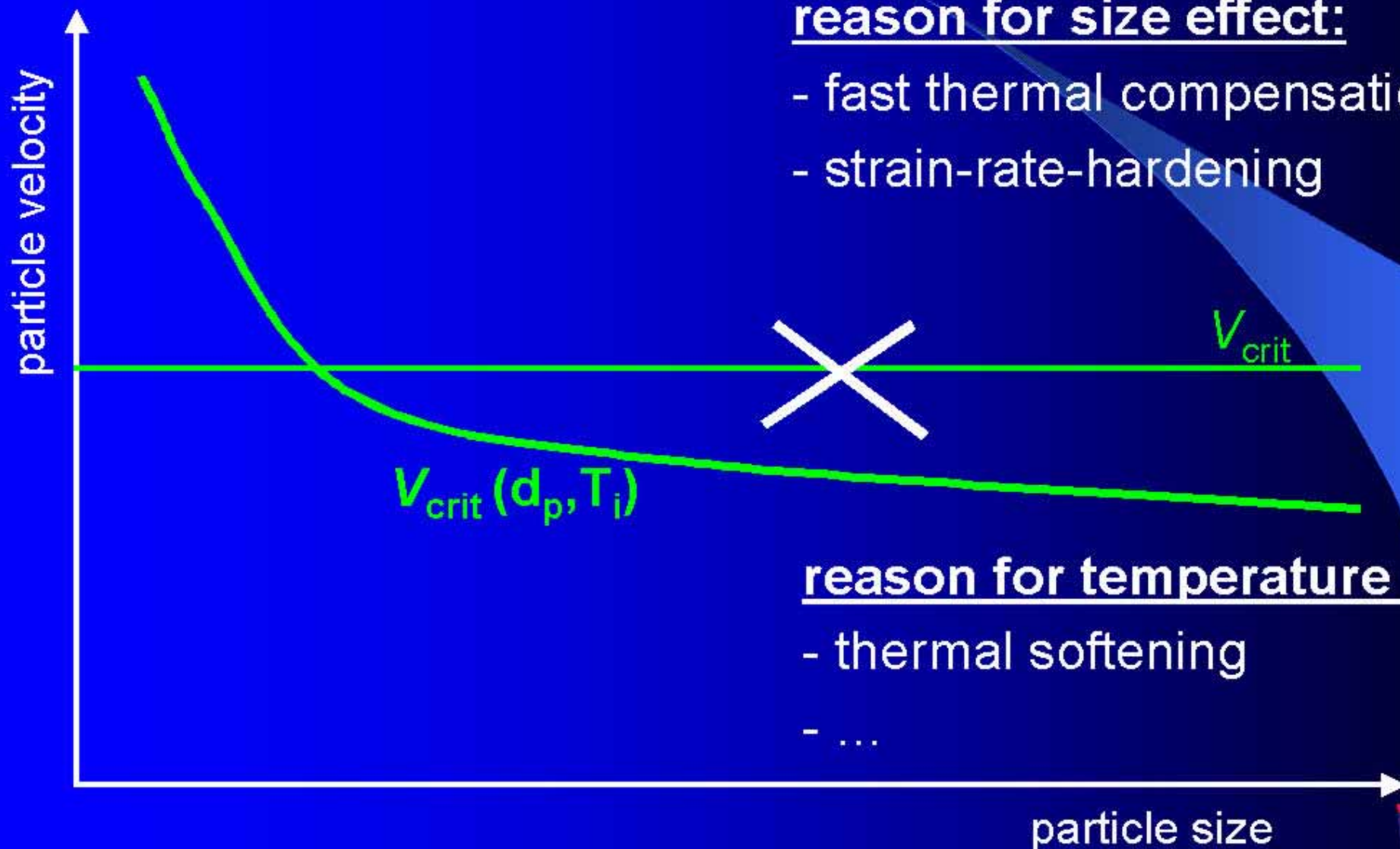
- lower cooling rate
- interfacial heating is more effective

Interface Temperature → Critical Velocity [3, 5]

interface temperature as a function of impact velocity



Critical Velocity is a Function of Particle Size and Particle Impact Temperature



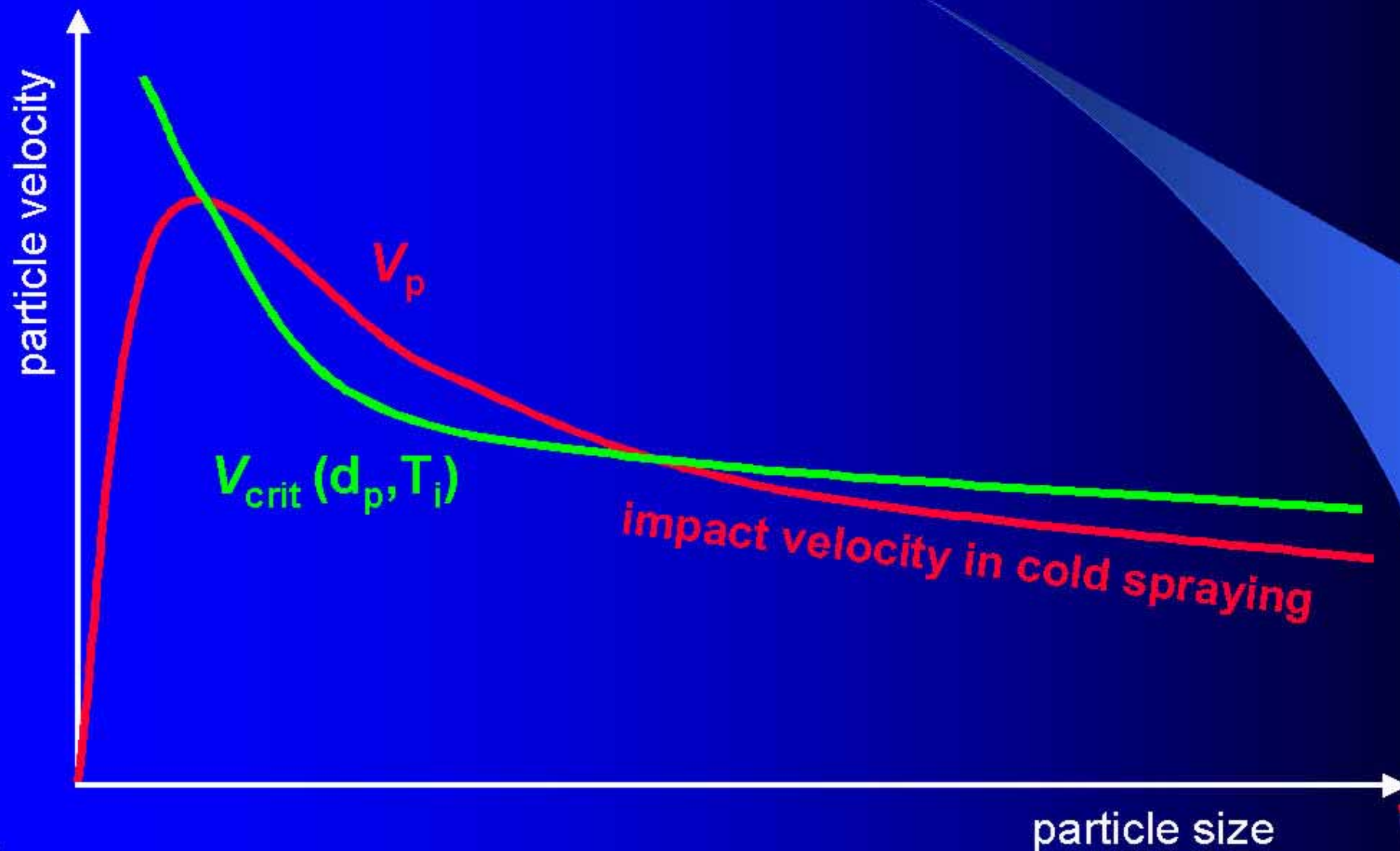
reason for size effect:

- fast thermal compensation
- strain-rate-hardening

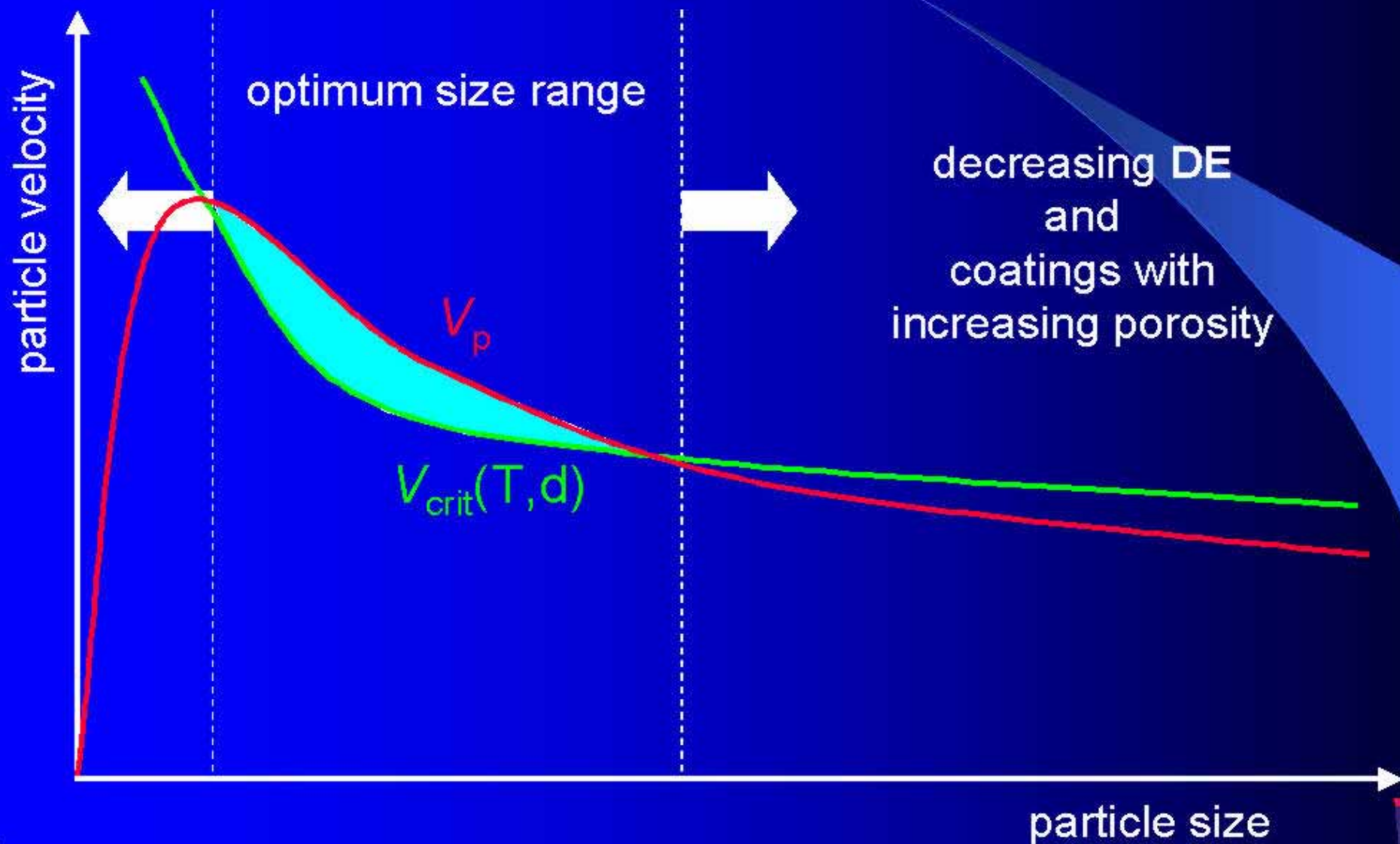
reason for temperature effect:

- thermal softening
- ...

Critical Velocity and Impact Velocity for a certain Spray Parameter

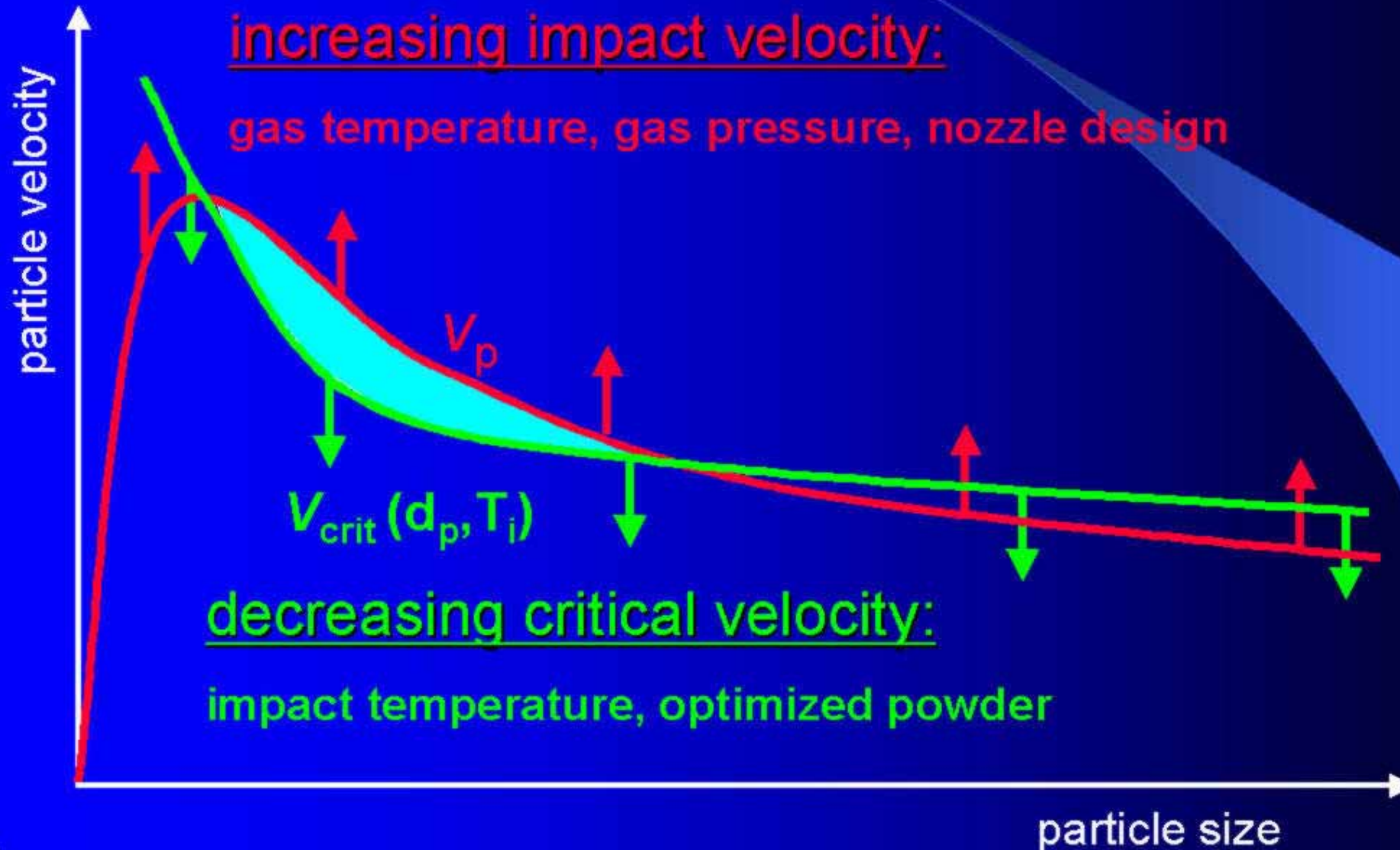


Critical Velocity and Impact Velocity [3] for a certain Spray Parameter



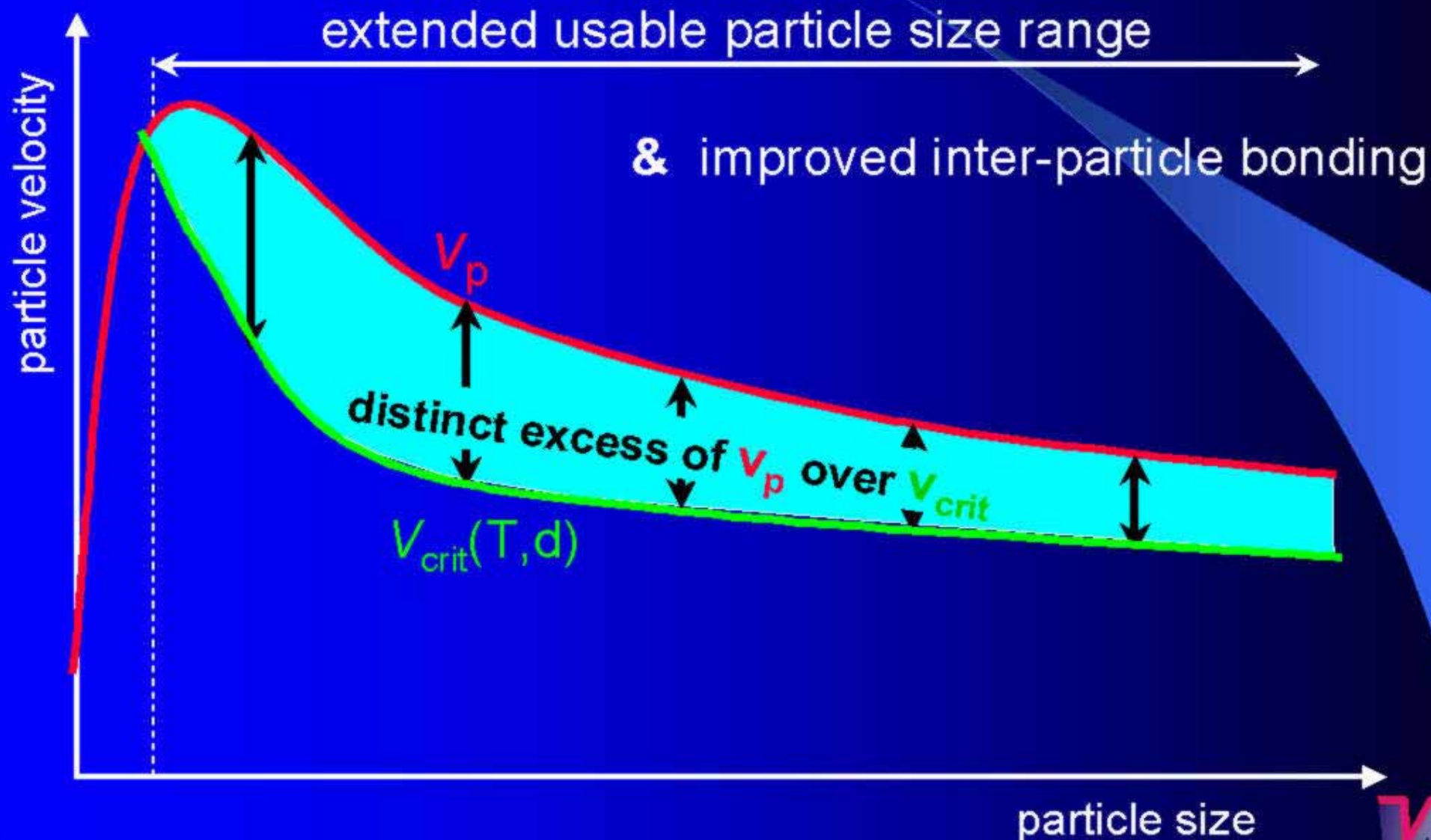
Concept of Process Optimization:

distinct excess of **impact velocity** over **critical velocity**



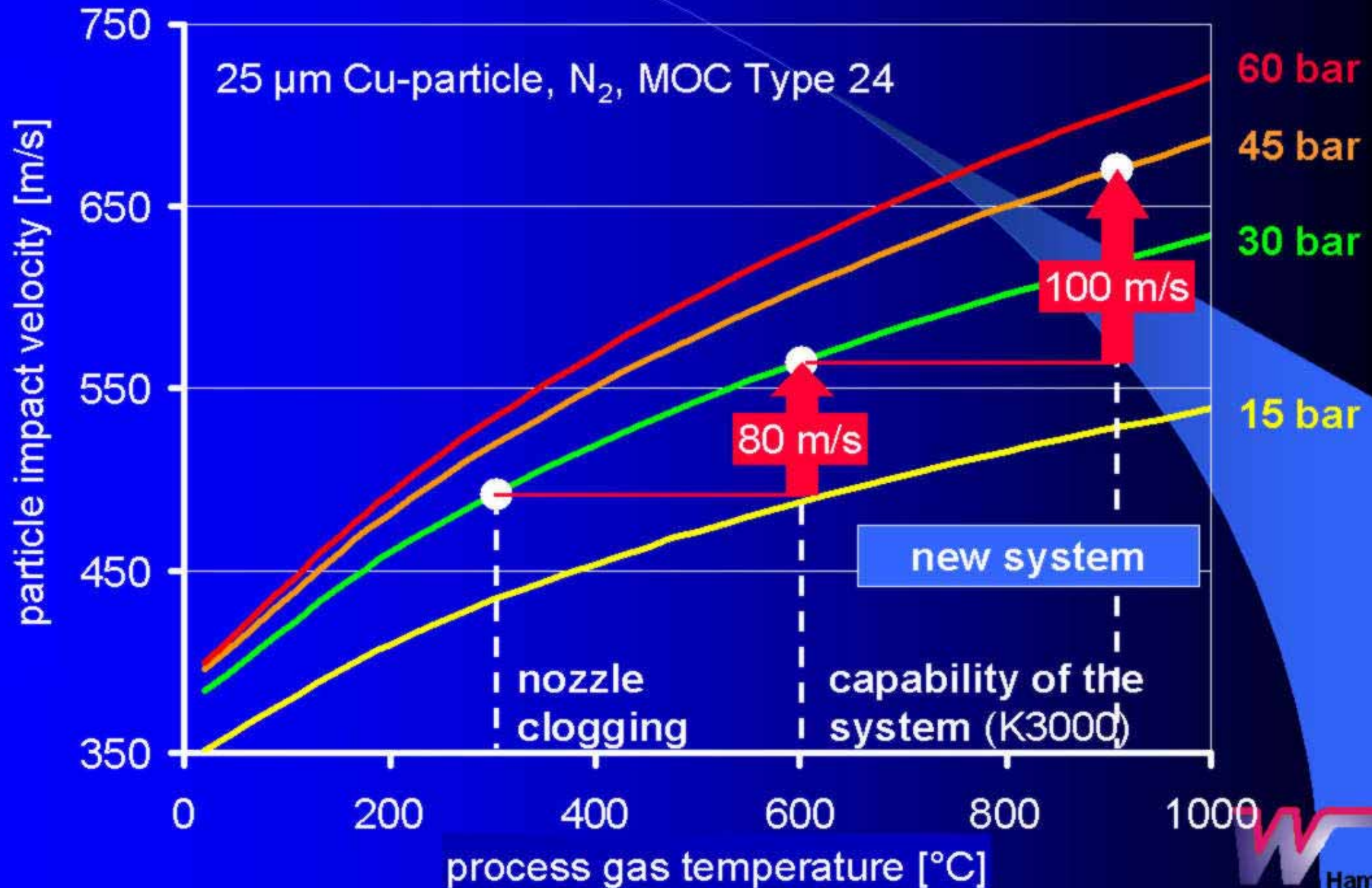
Aim of Process Optimization:

extended particle size range & improved particle bonding



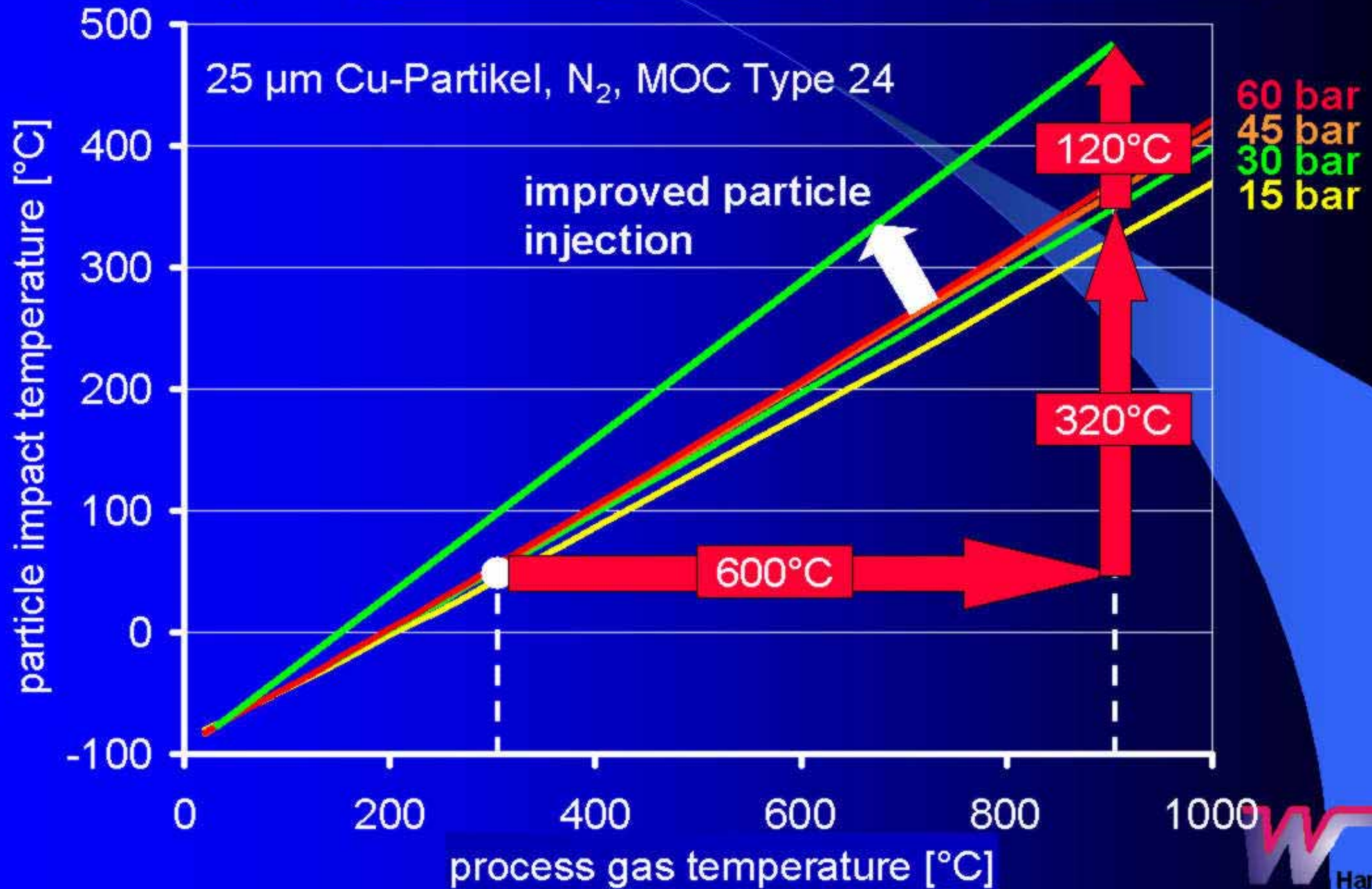
Higher Impact Velocity

by higher gas pressure and temperature



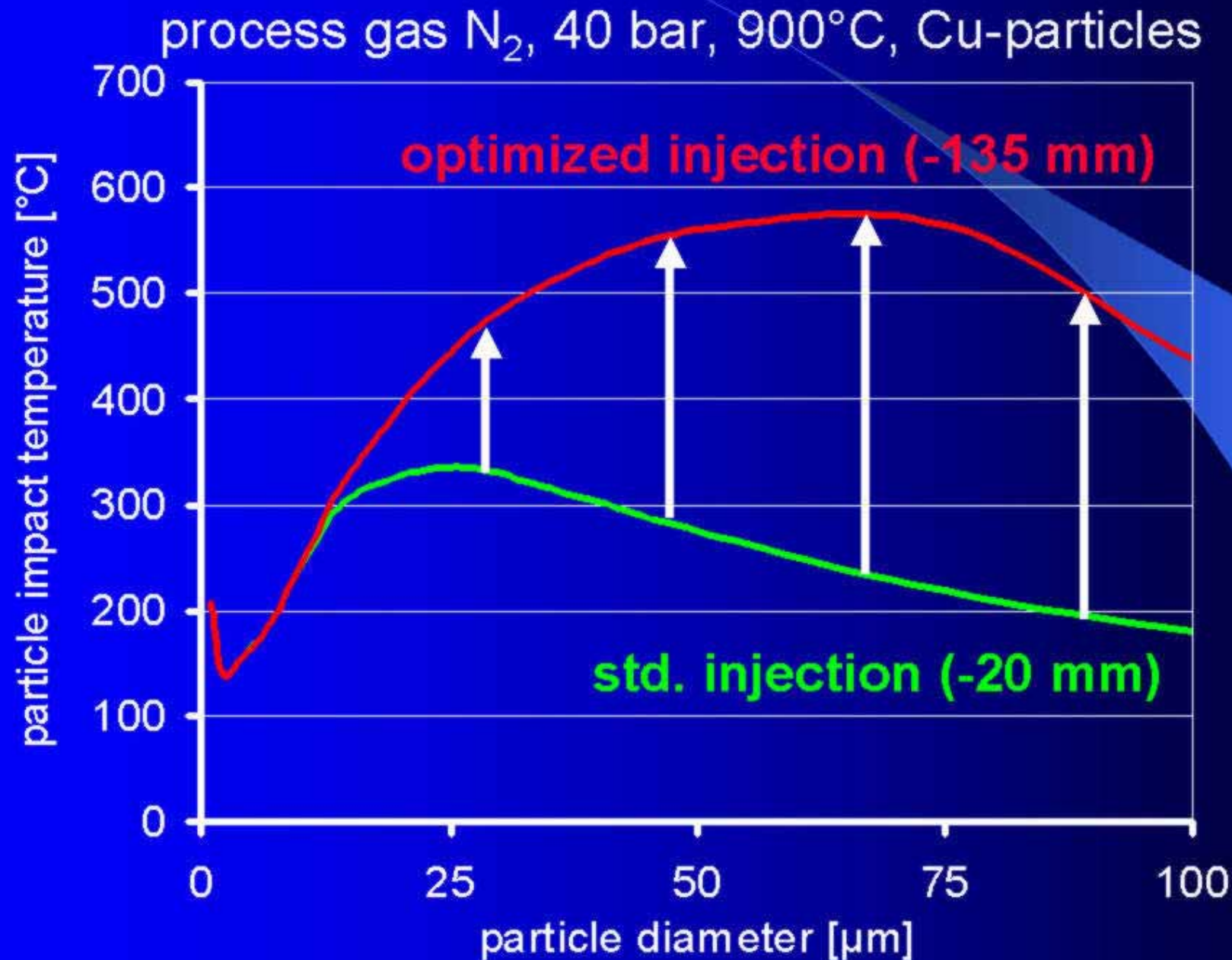
Higher Impact Temperature

by higher gas temperature and preheating



Optimized Particle Injection (Preheating) [4, 5]

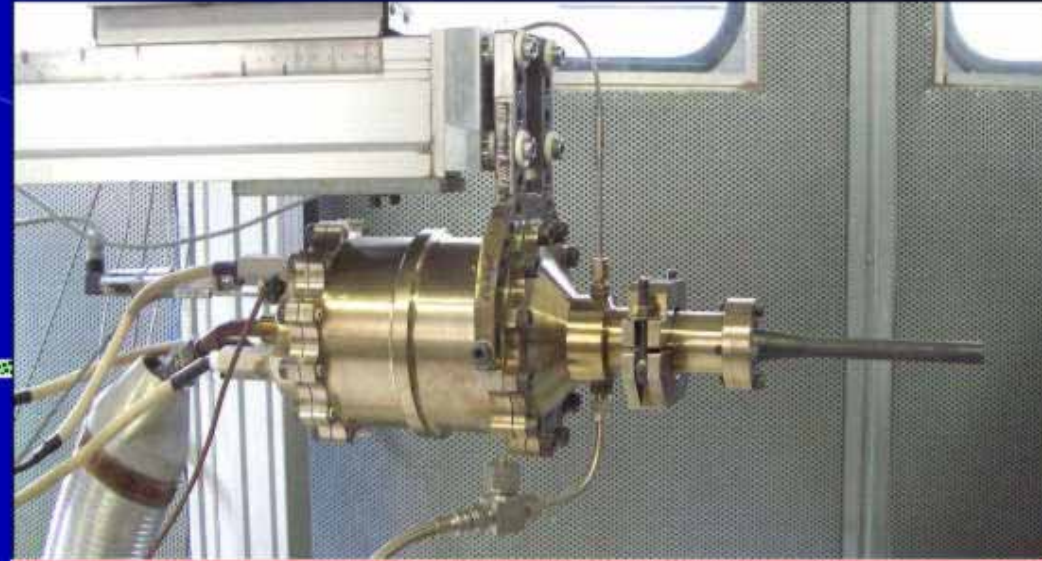
>> higher impact temperatures



System for Extended Conditions [4, 5]:

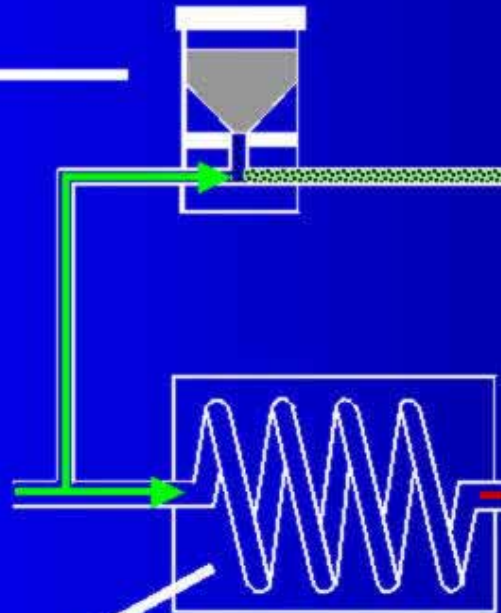


powder feeder
45 bar



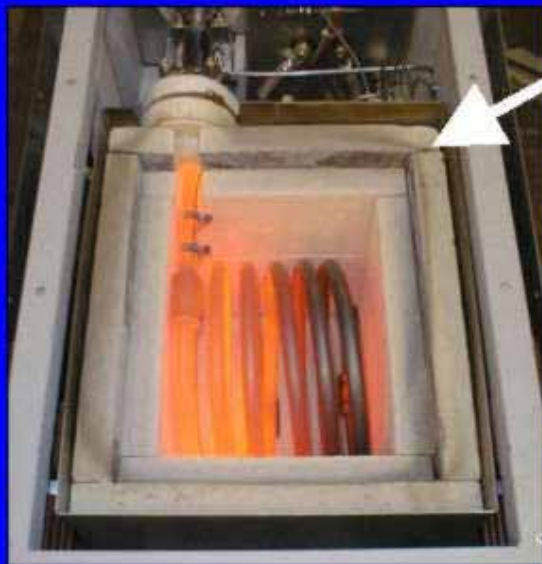
New spray gun with 17 kW heater
40 bar, 900 °C

gas supply
45 bar



heater:

~ 25 kW, 650 °C

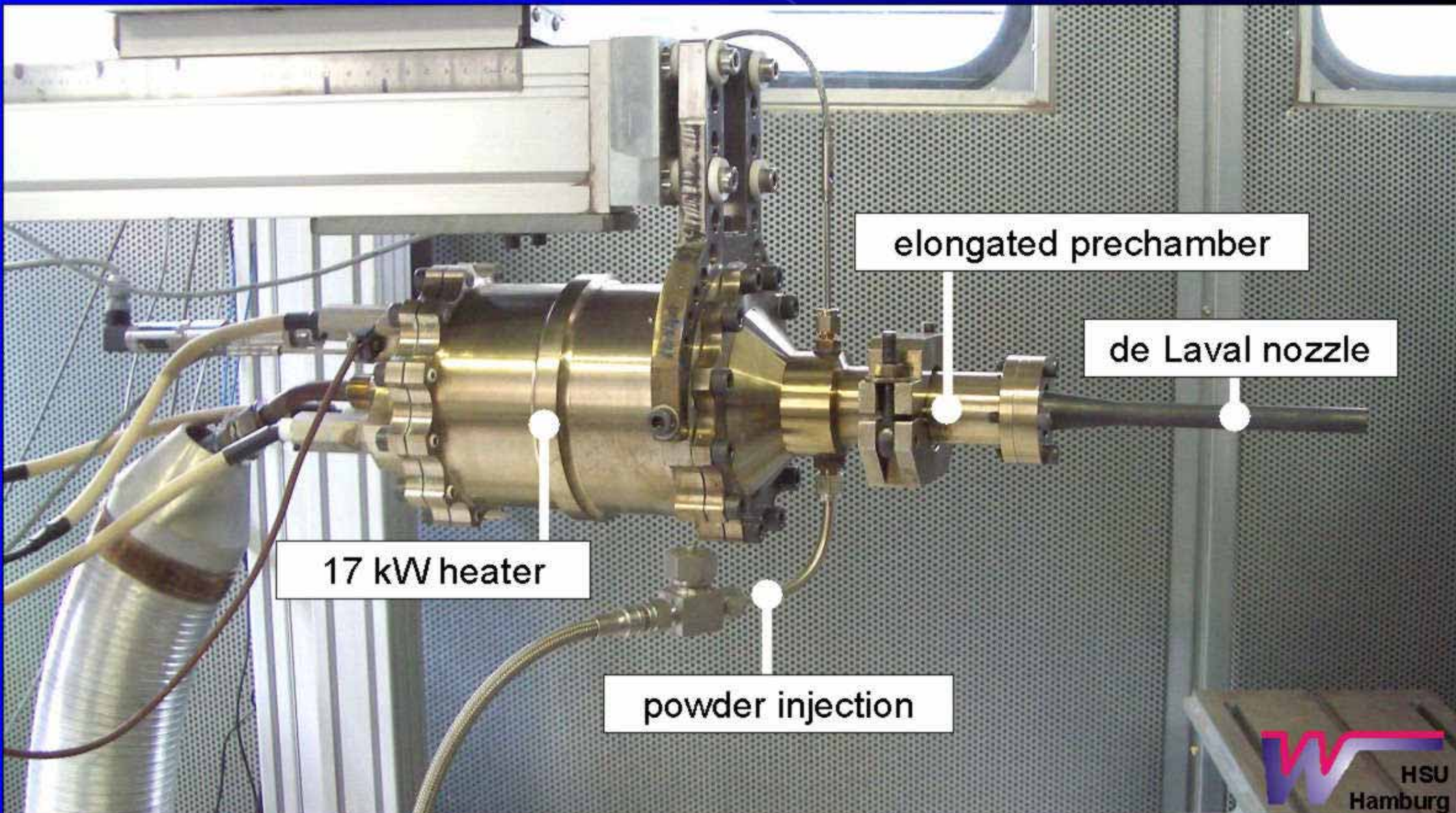


wide range of process conditions:

✓ flexible range of impact conditions

New Spray Gun Developed at HSU Hamburg

prototype of the "Active Jet of K4000"

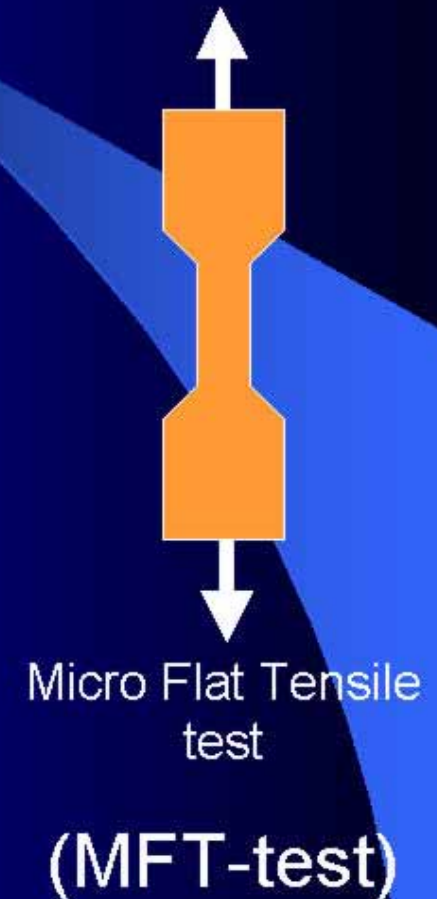


Investigation of Inter-Particle Bonding

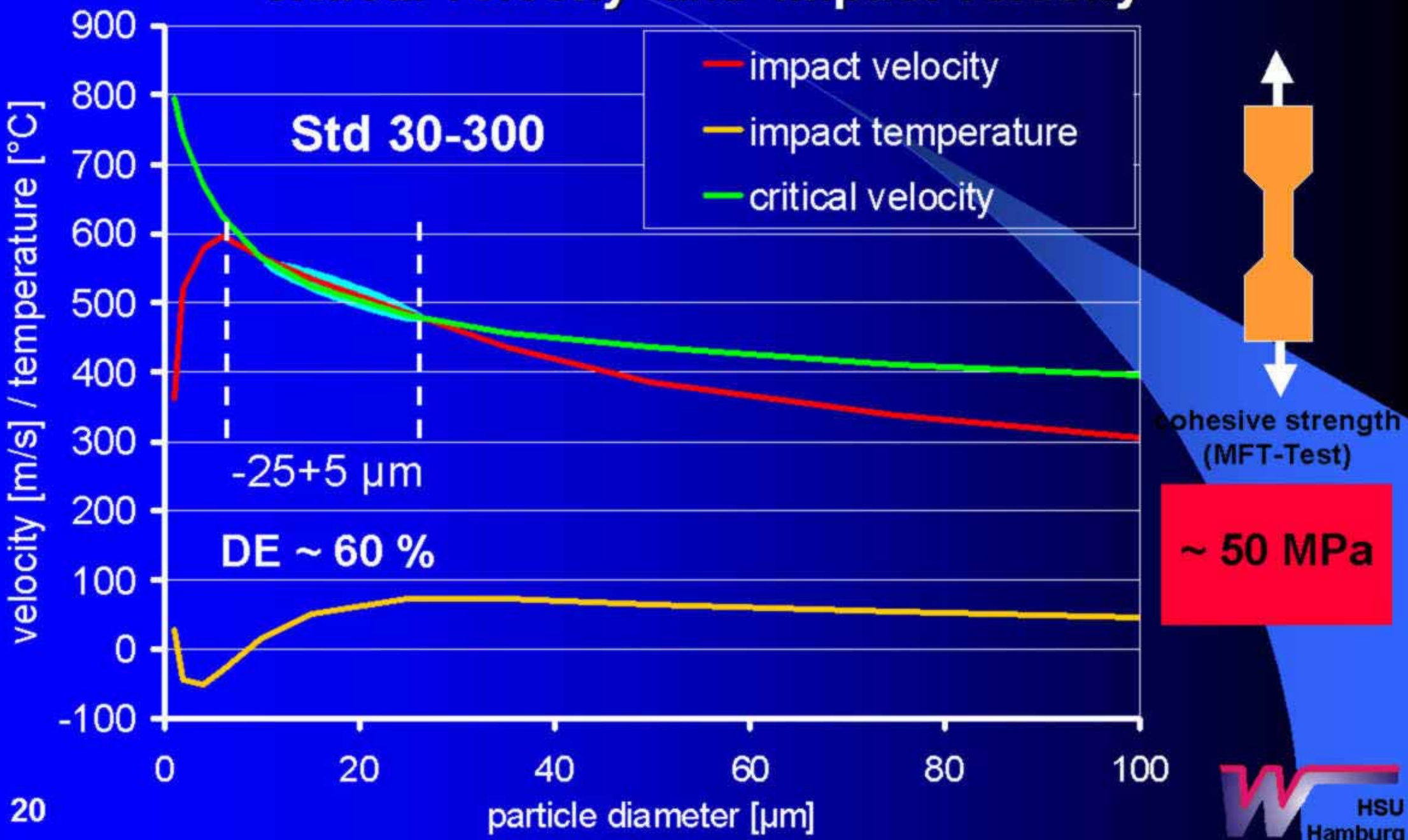
Micro-Flat-Tensile-Test (MFT-test), strength and ductility of coatings

Micro Tensile Sample:

sample preparation:	spark erosion
initial coating thickness:	2 - 3 mm
sample size:	28 mm x 5 mm x 1 mm
gauge length:	9 mm
strain measurement:	laser extensometer

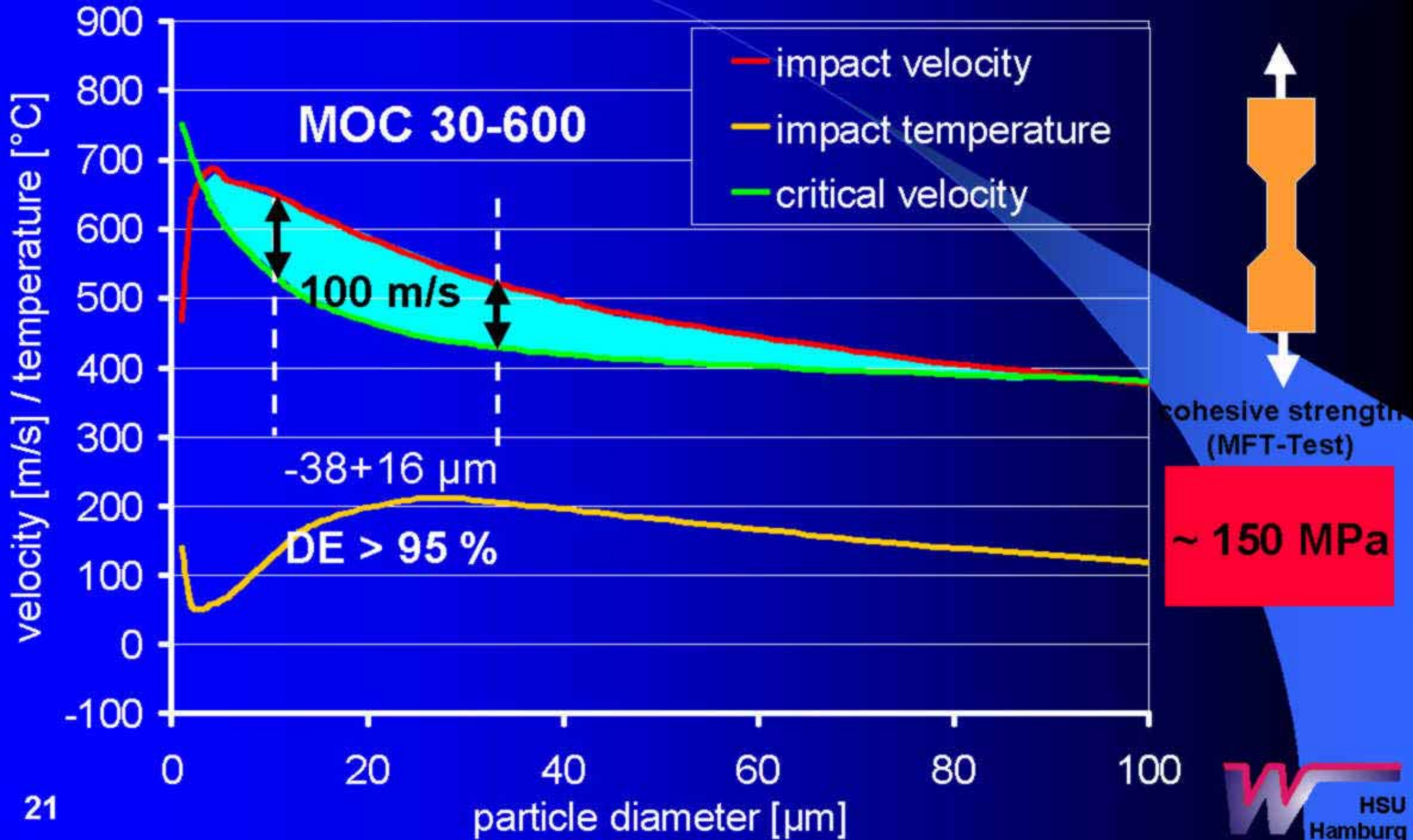


Cold Spraying of Copper, State 2001 [4, 5] critical velocity and impact velocity



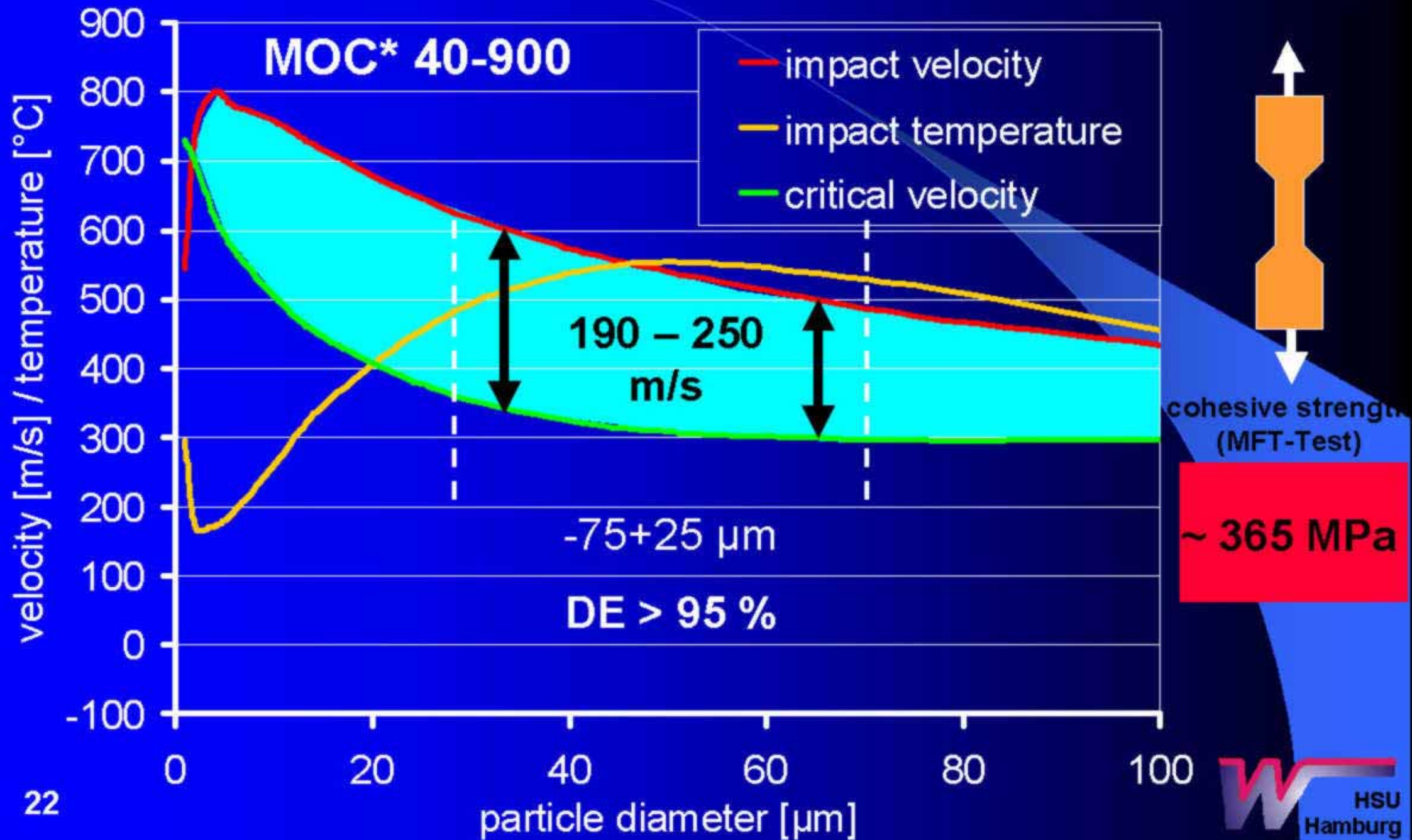
Cold Spraying of Copper, State 2004 [4, 5]

distinct exceeding of critical velocity by impact velocity



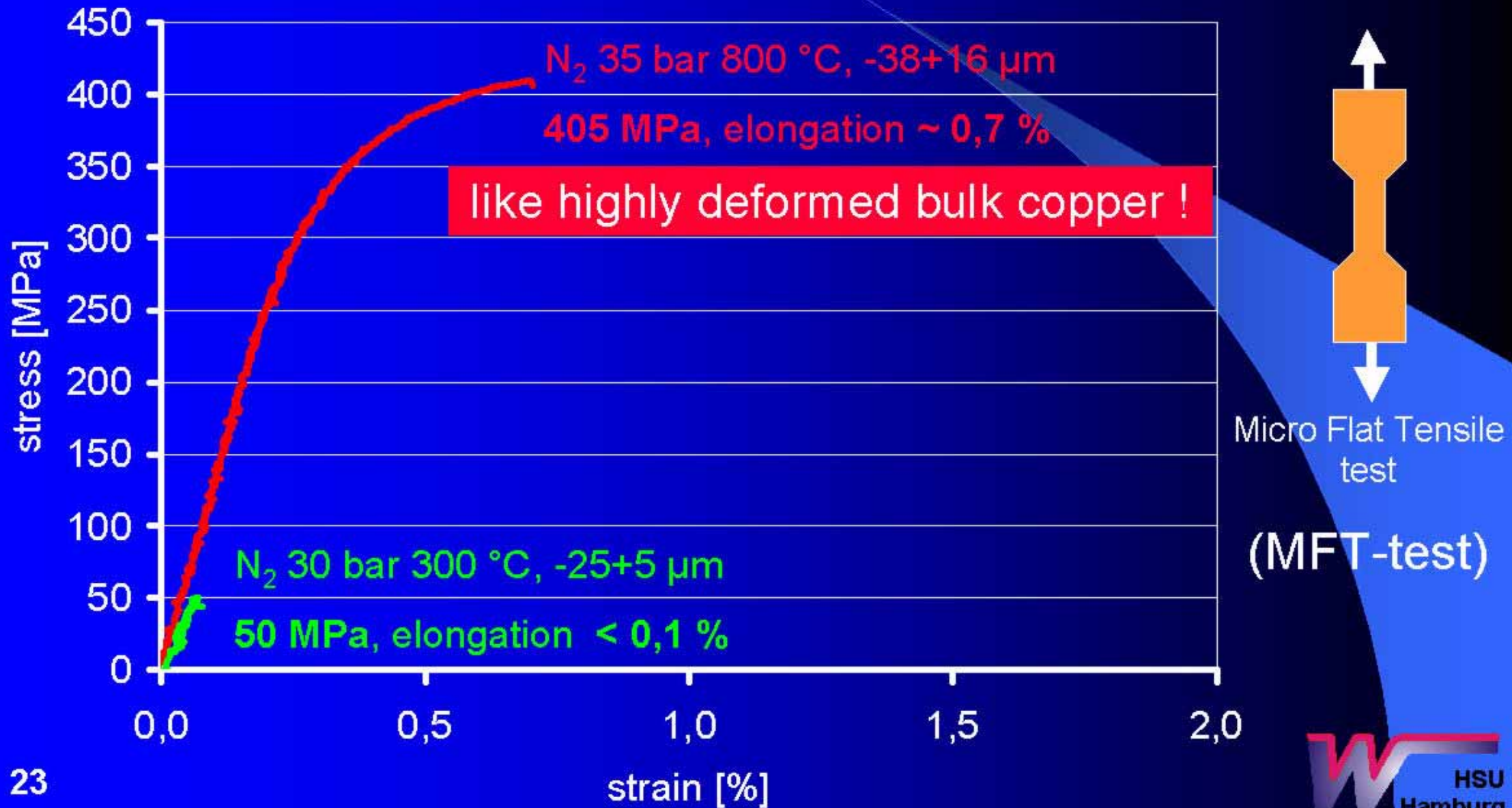
Cold Spraying of Copper, State 2007 [4, 5]

distinct exceeding of critical velocity by impact velocity



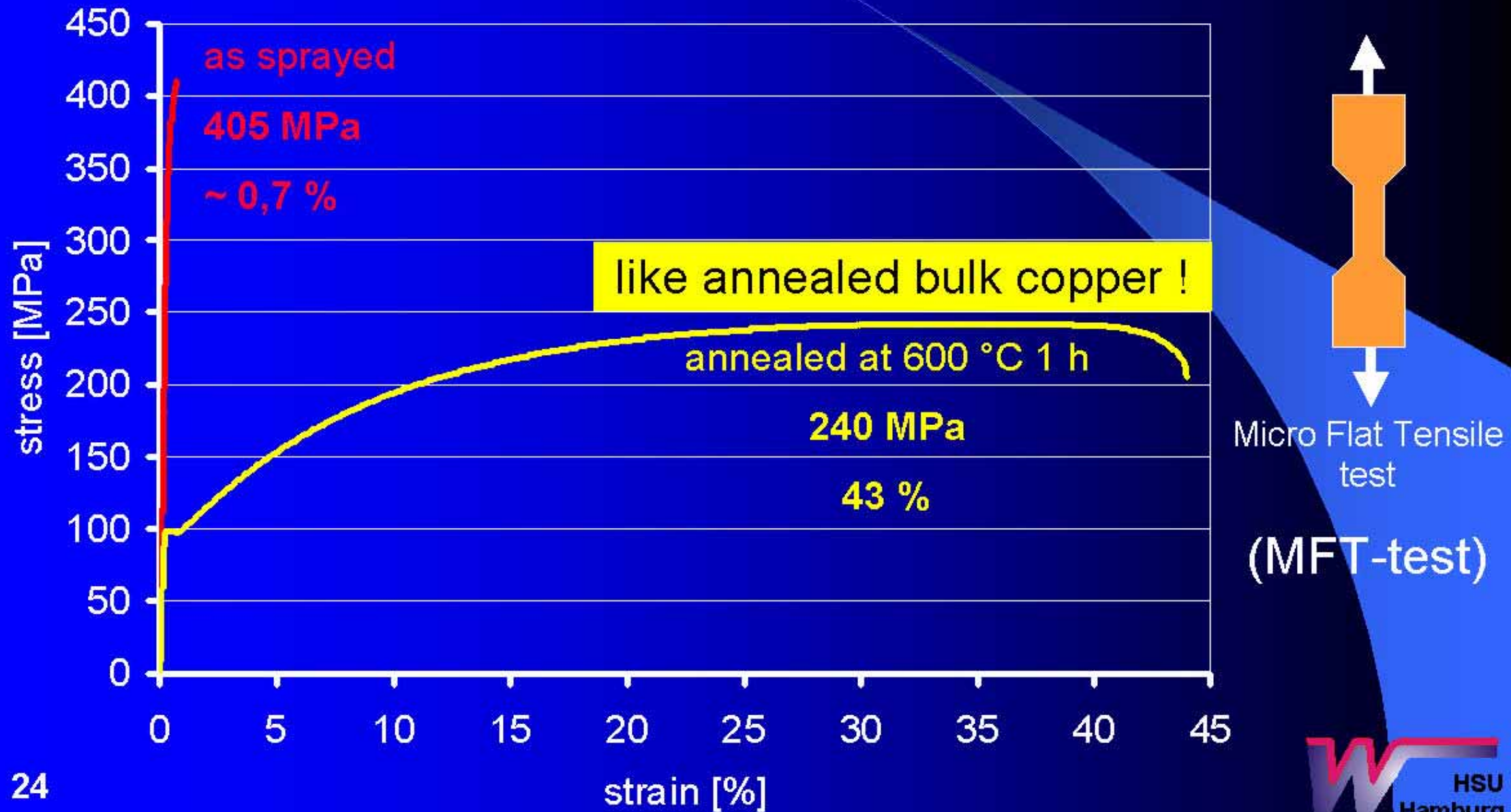
Strength and Ductility, MFT-Test [4, 5]

old and new parameter setting for Cu

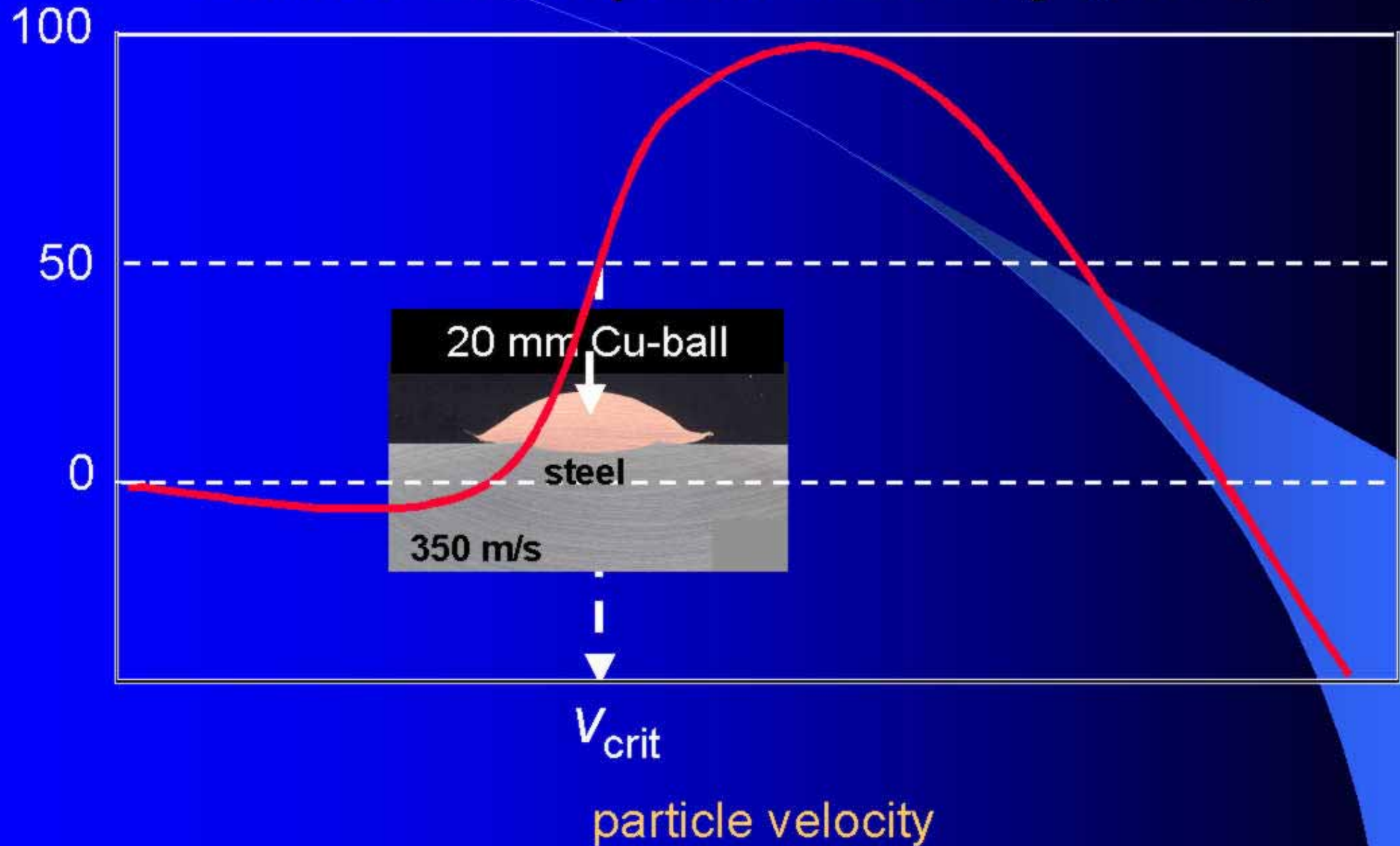


Strength and Ductility, MFT-Test [4, 5]

new parameter setting for Cu, coating annealed



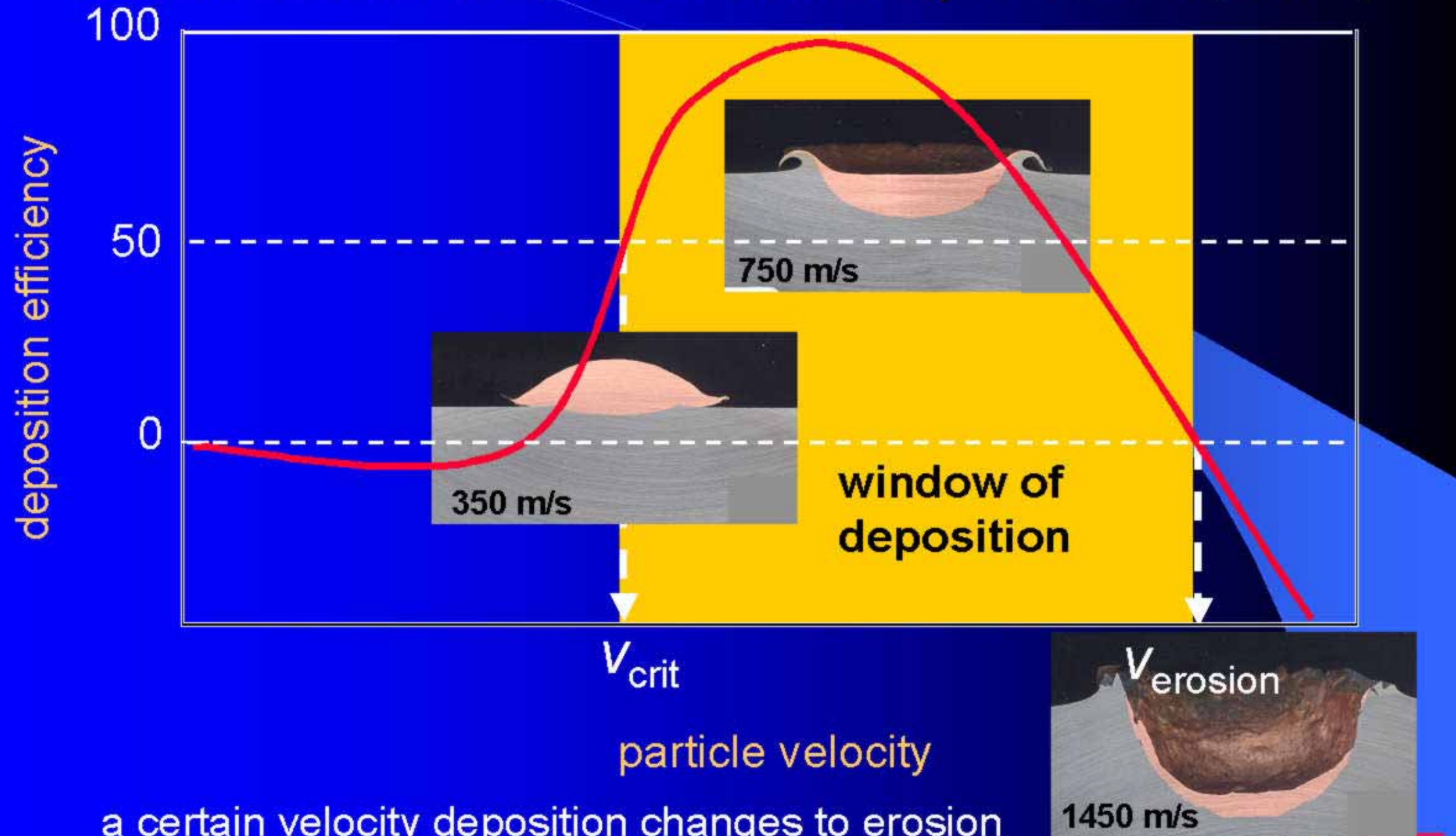
Effect of Impact Velocity [3, 4, 5]



at a certain velocity particles start to stick

✓ at a DE of 50 % the critical velocity is defined

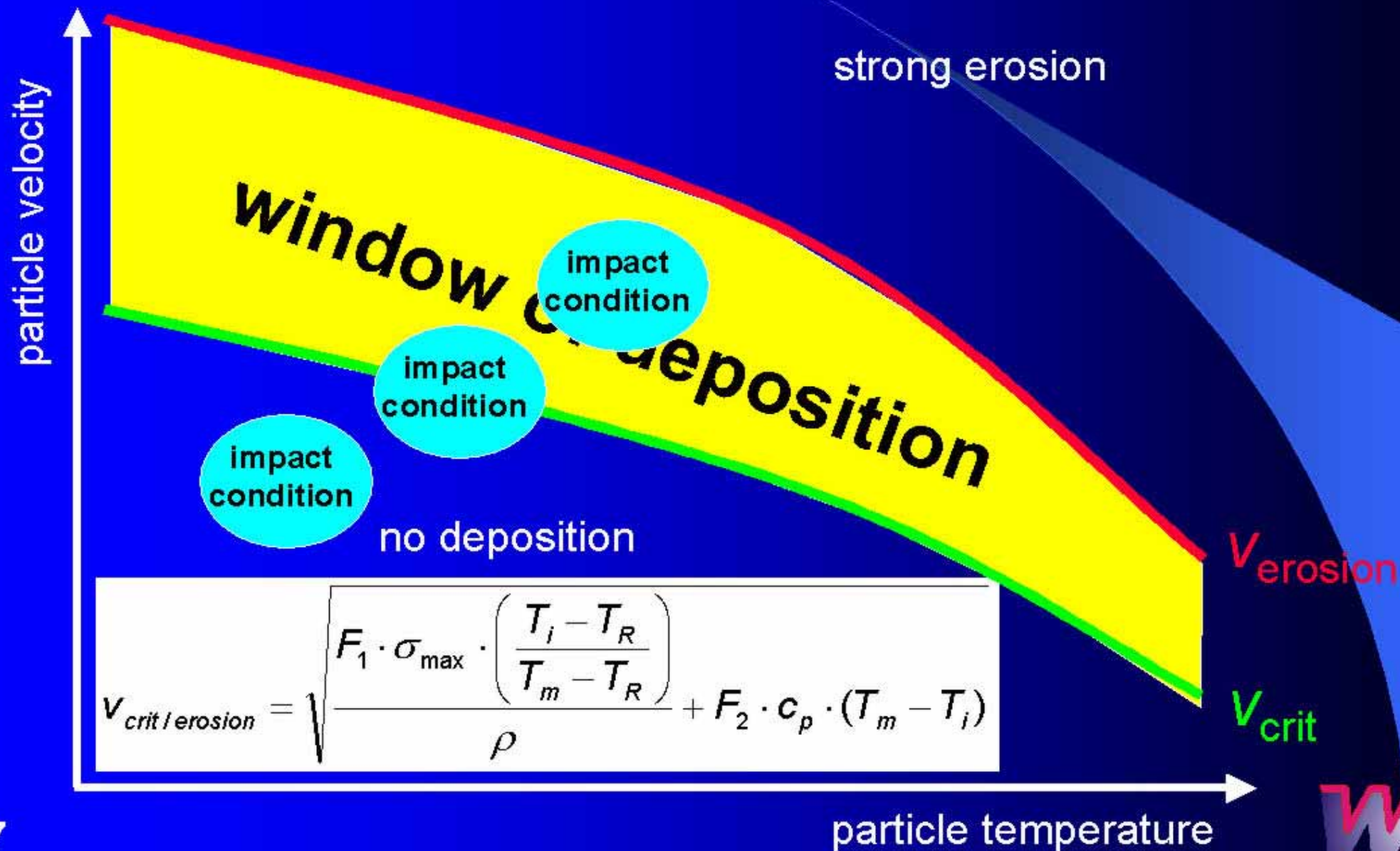
Parameter Window for Deposition [3, 4, 5]



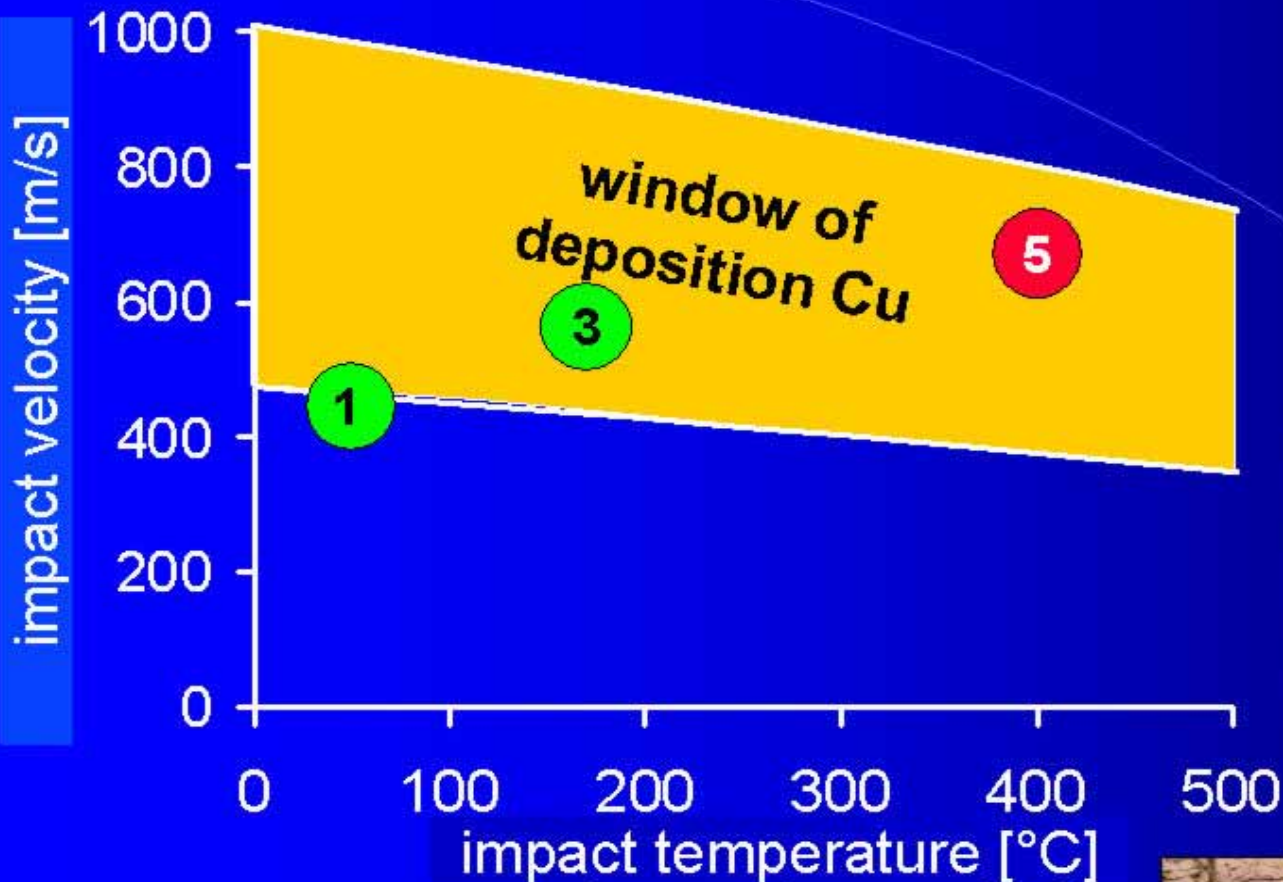
a certain velocity deposition changes to erosion

Parameter Window for Deposition [3]

prediction of optimal impact conditions



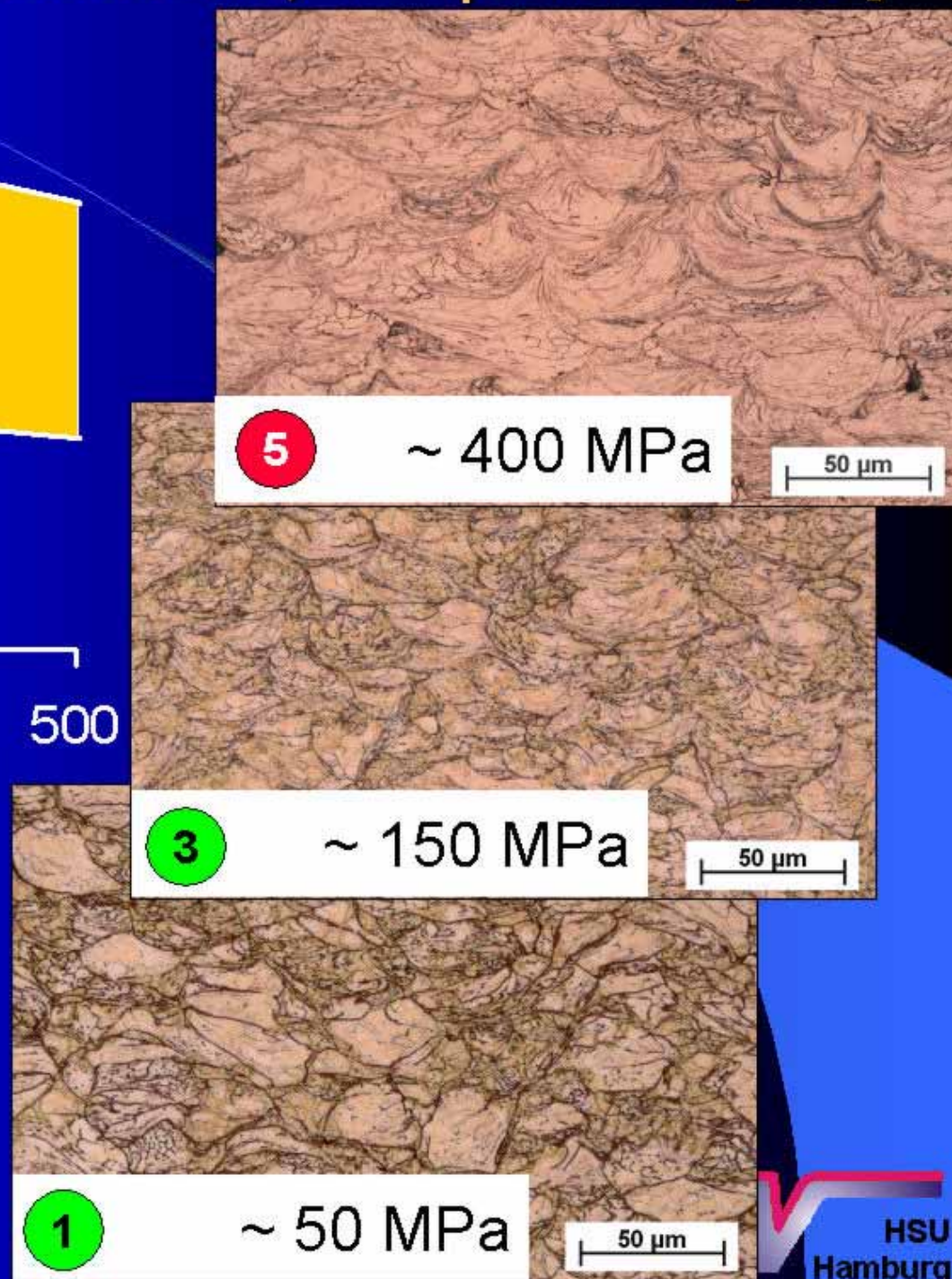
Impact Conditions, Microstructure, Properties [4, 5]



Kinetiks 3000:

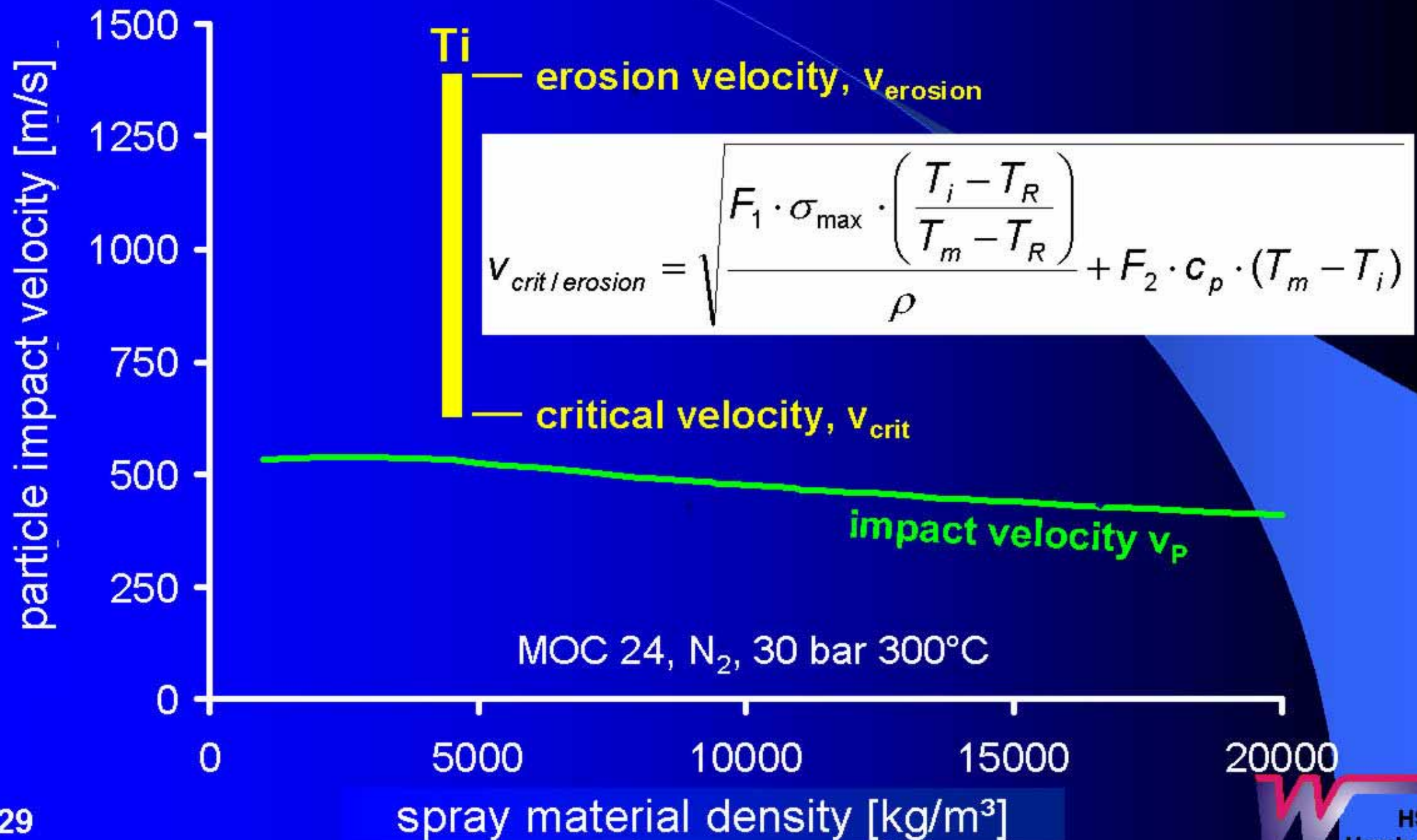
- 1: steel nozzle Type 2 (2001)
- 3: WCCo nozzle Type 24 (2004)

- New Equipment (Kinetiks 4000):
- 5: new spray gun (2006)



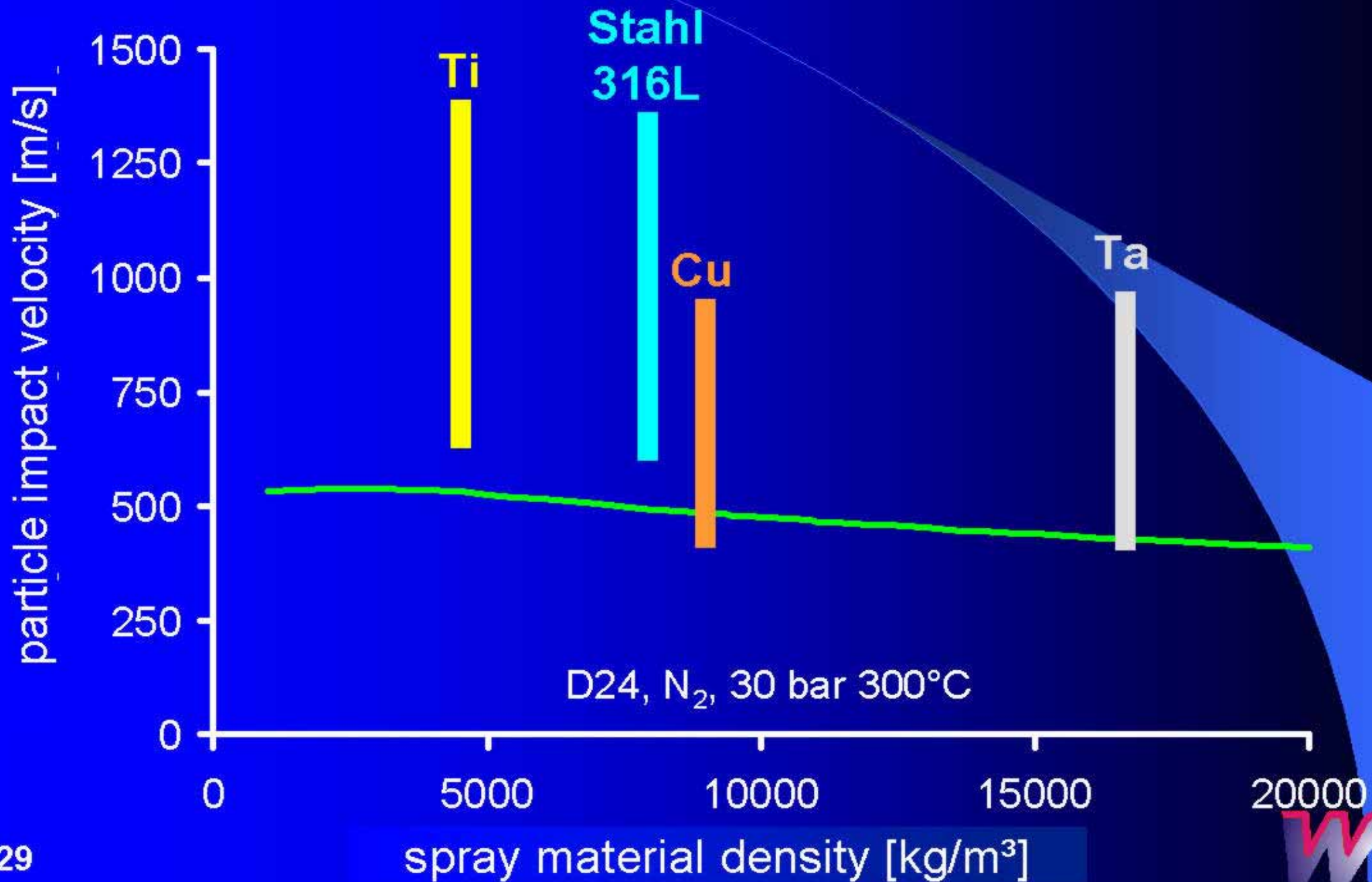
Window for Deposition [3, 5]

transfer of results to other materials, calculated for 25 μm particles



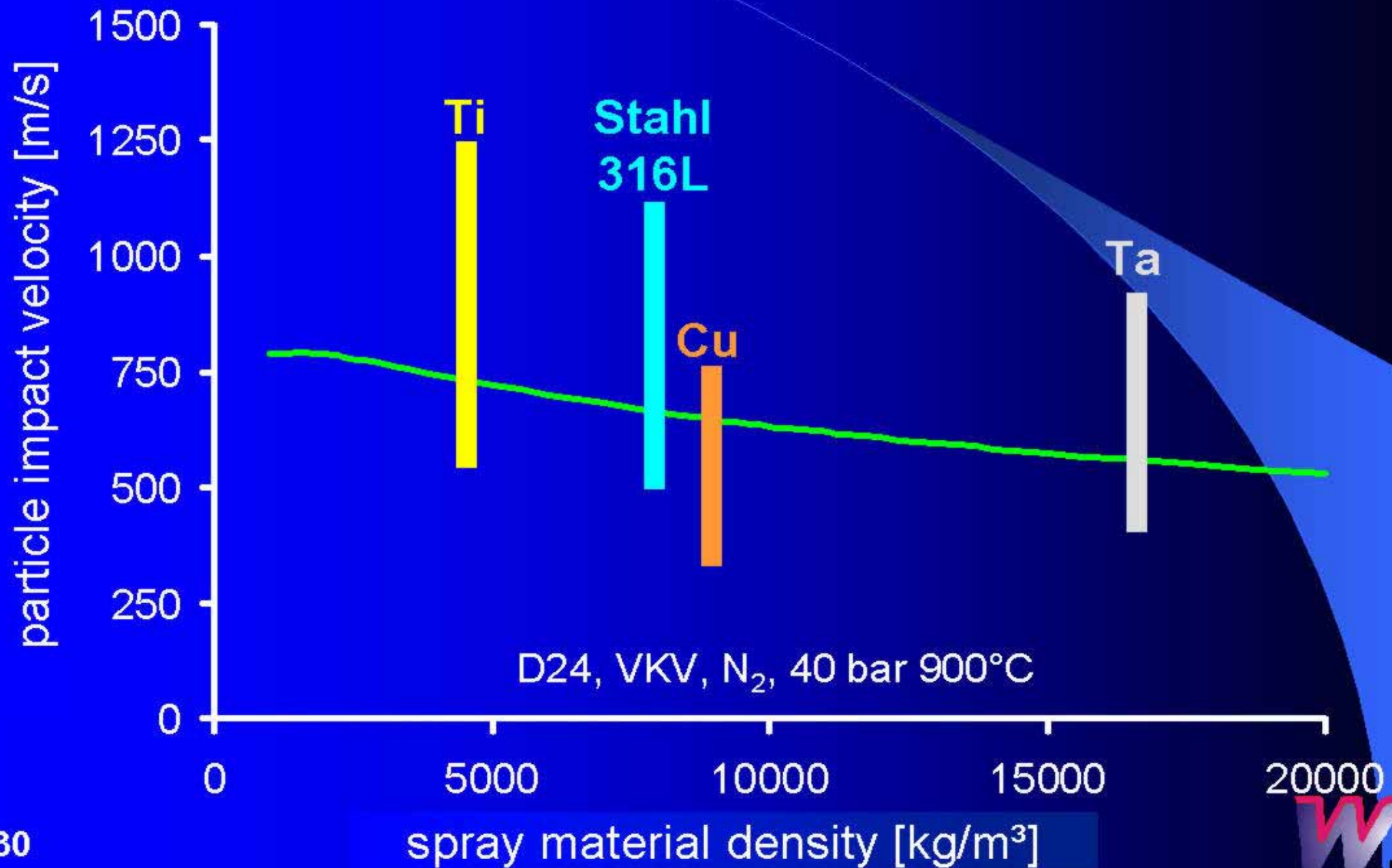
Window for Deposition, State 2001 [5]

transfer of results to other materials, calculated for 25 μm particles



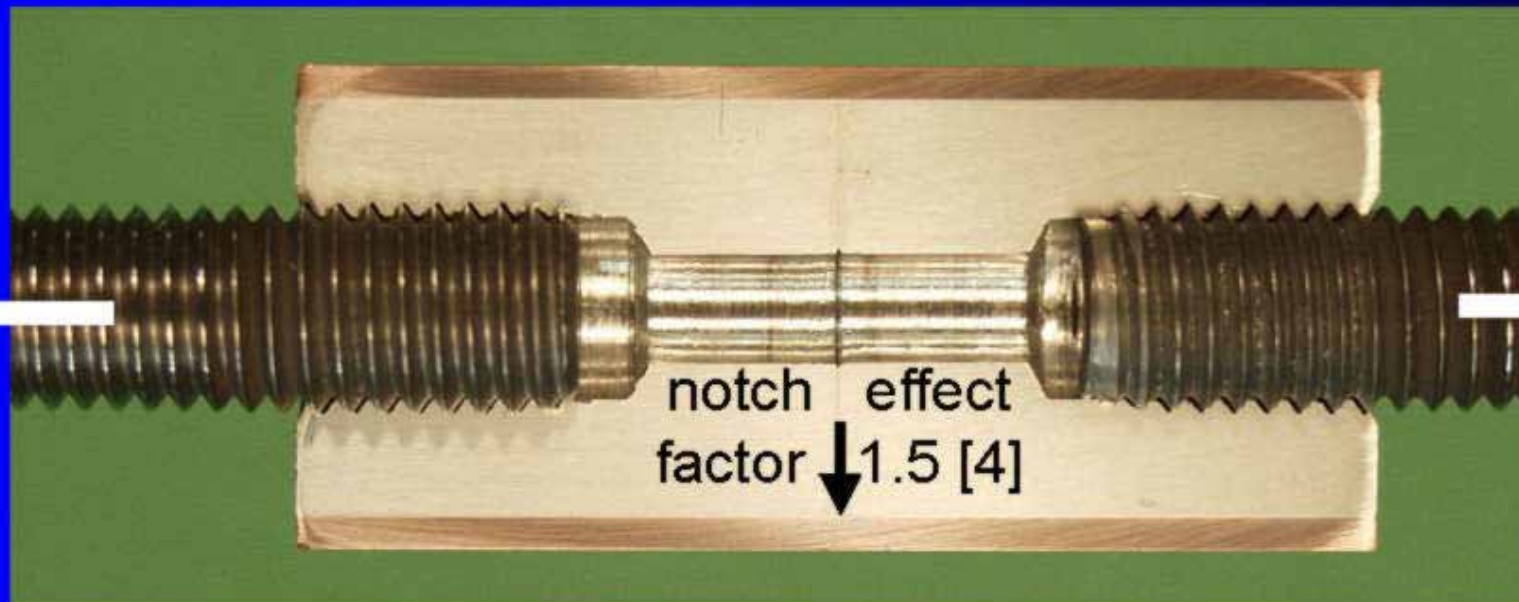
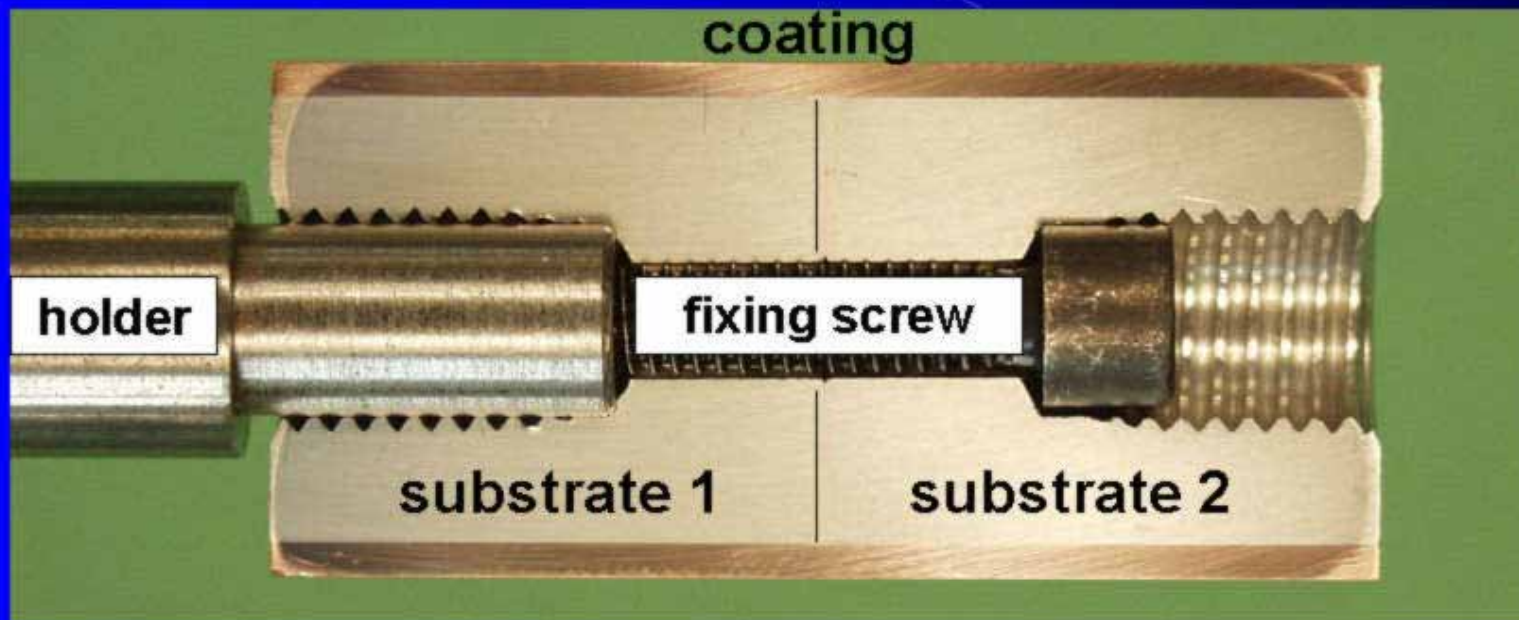
Window for Deposition, State 2007 [5]

transfer of results to other materials, calculated for 25 μm particles



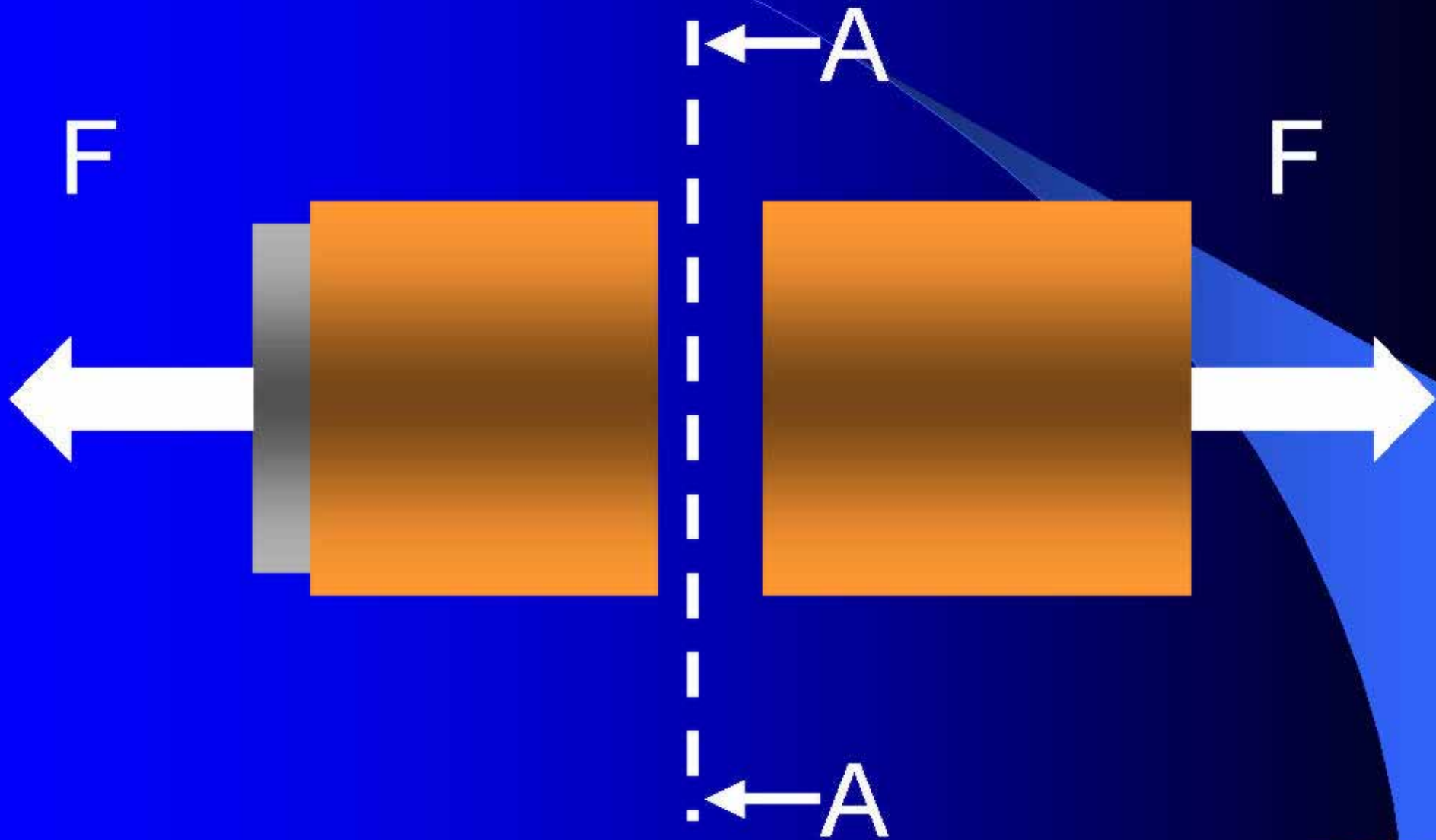
Cohesive Strength of Coatings [3, 4, 5]

Tubular-Coating-Tensile-Test (TCT-Test)



Cohesive Strength of Coatings

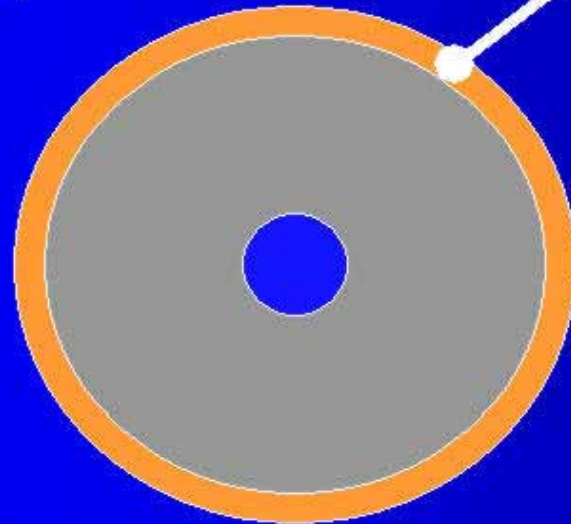
Tubular-Coating-Tensile-Test (TCT-Test)



Cohesive Strength of Coatings

Tubular-Coating-Tensile-Test (TCT-Test)

A - A



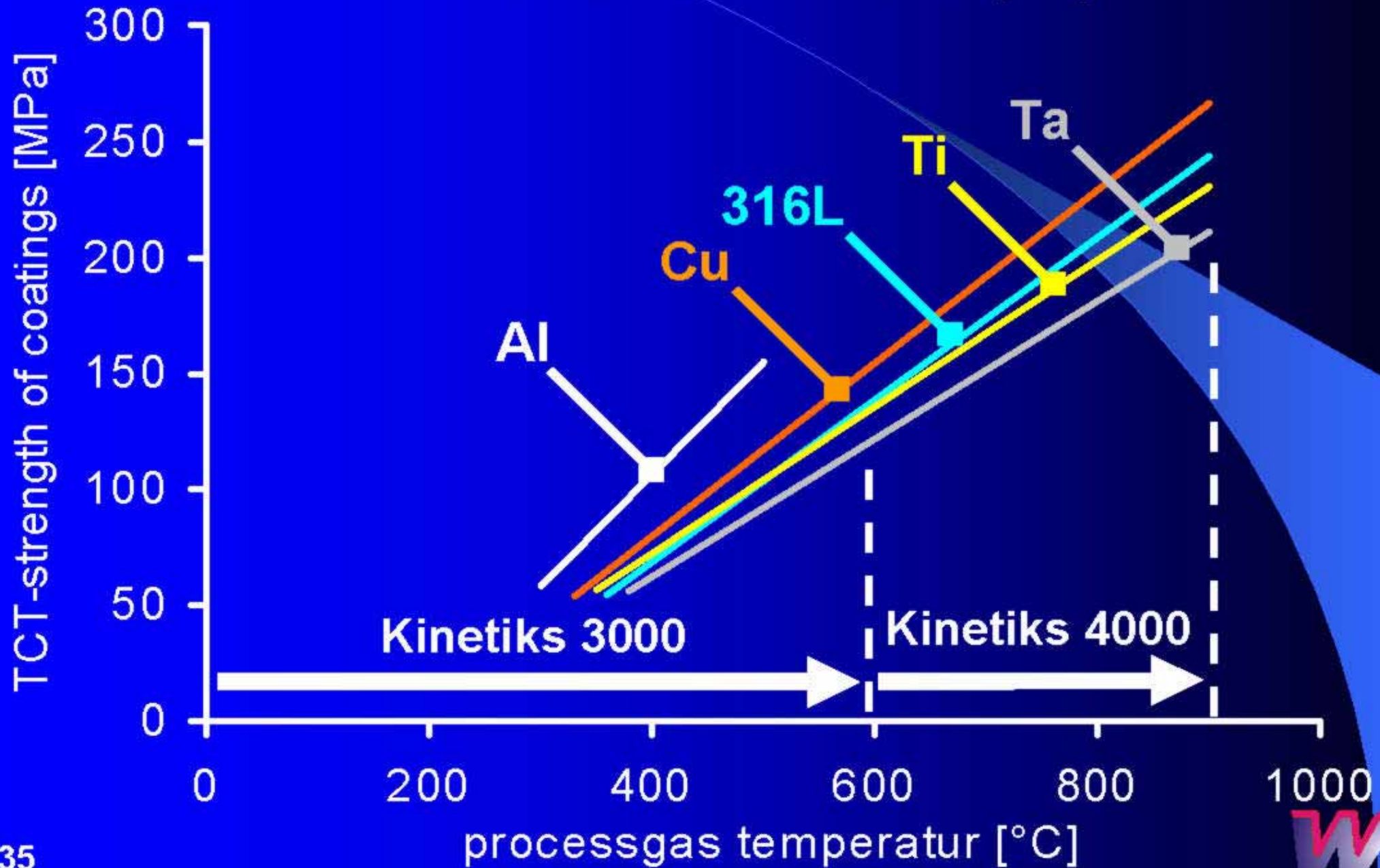
fracture
surface A

$$\sigma_{\text{TCT}} = F/A$$

advantages:

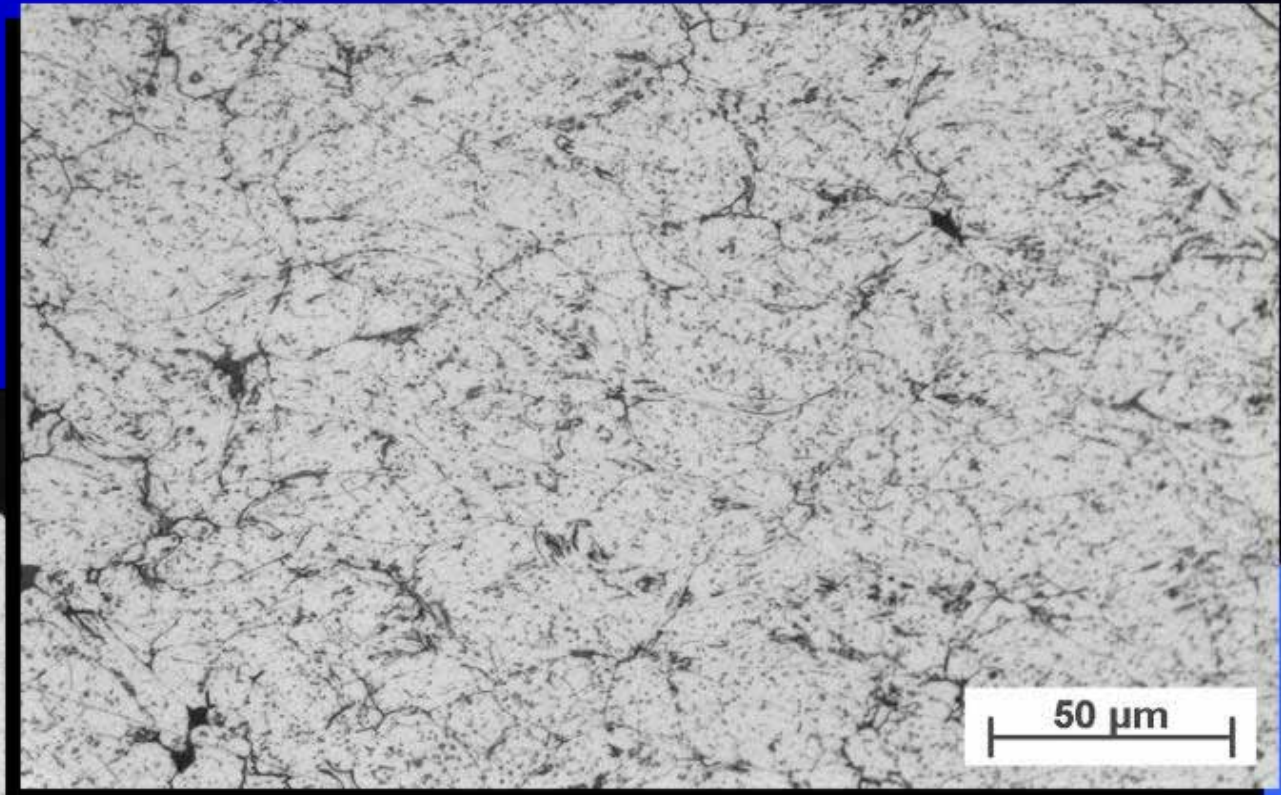
- ✓ easy to perform
- ✓ quick evaluation
- ✓ same equipment than for the bond strength
- ✓ ideal for process control and process optimization

Cohesive Strength of Coatings (TCT-Test) measured trend lines for different spray materials

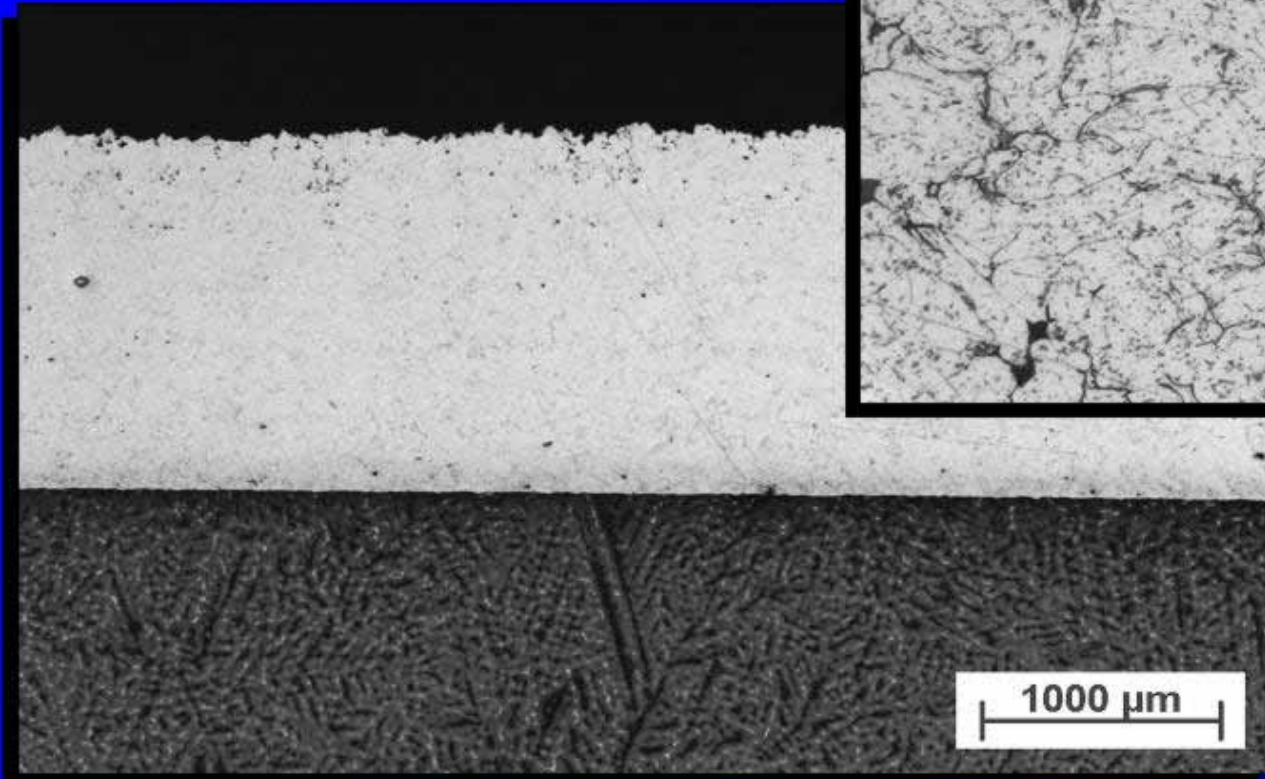


Al Coating (N₂)

TCT-test: 130 MPa

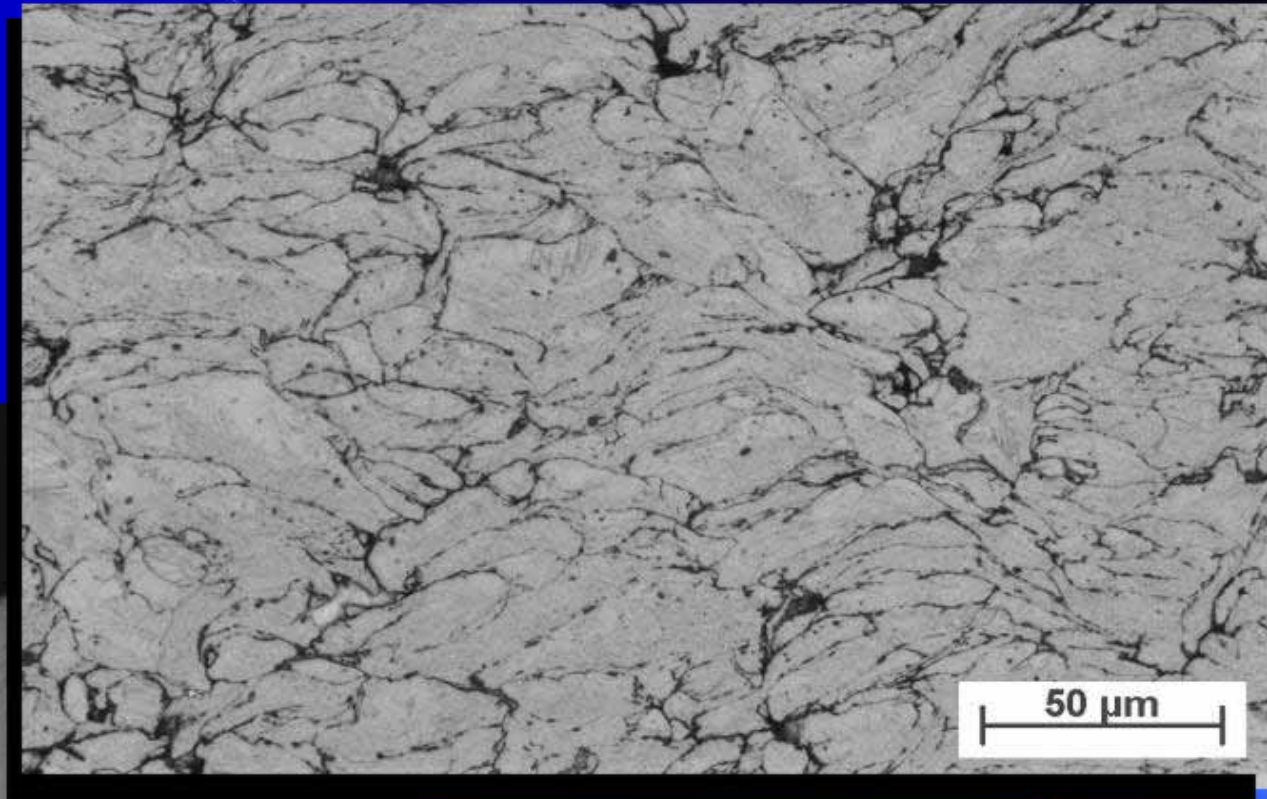


etched

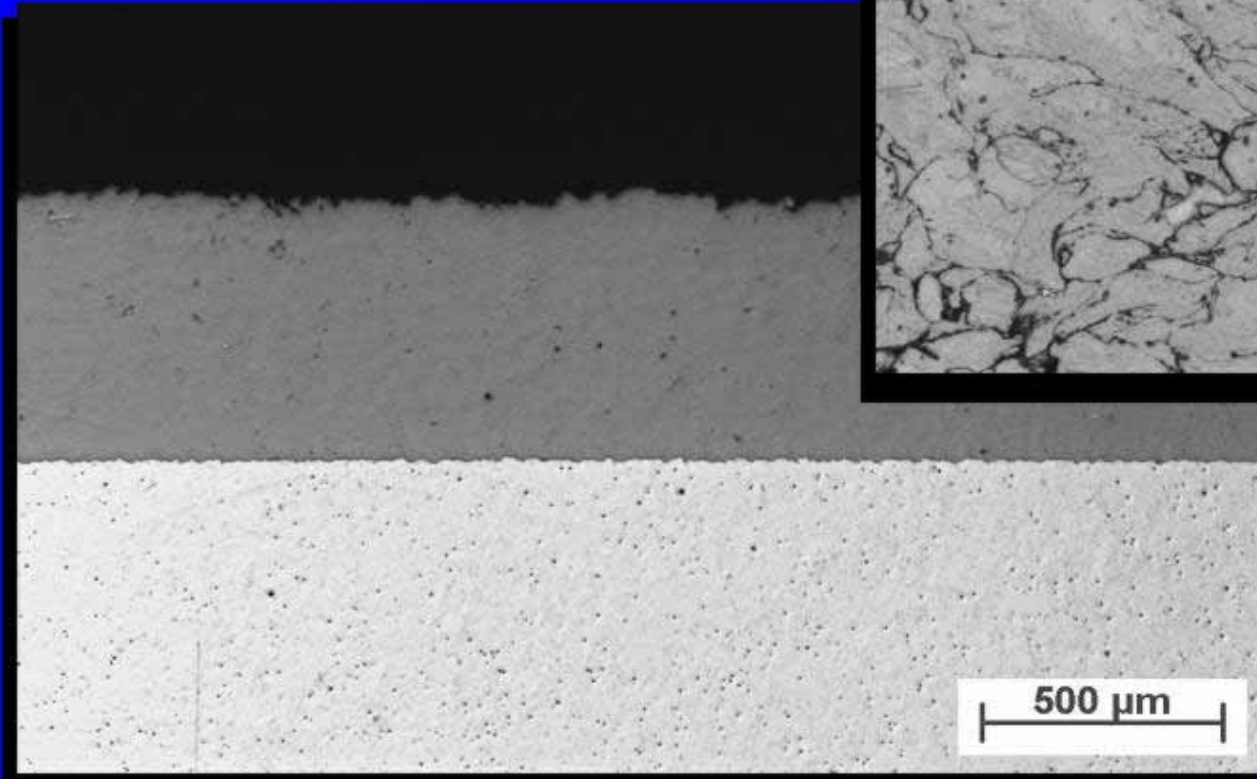


Ti Coating (N₂)

TCT-test: 225 MPa

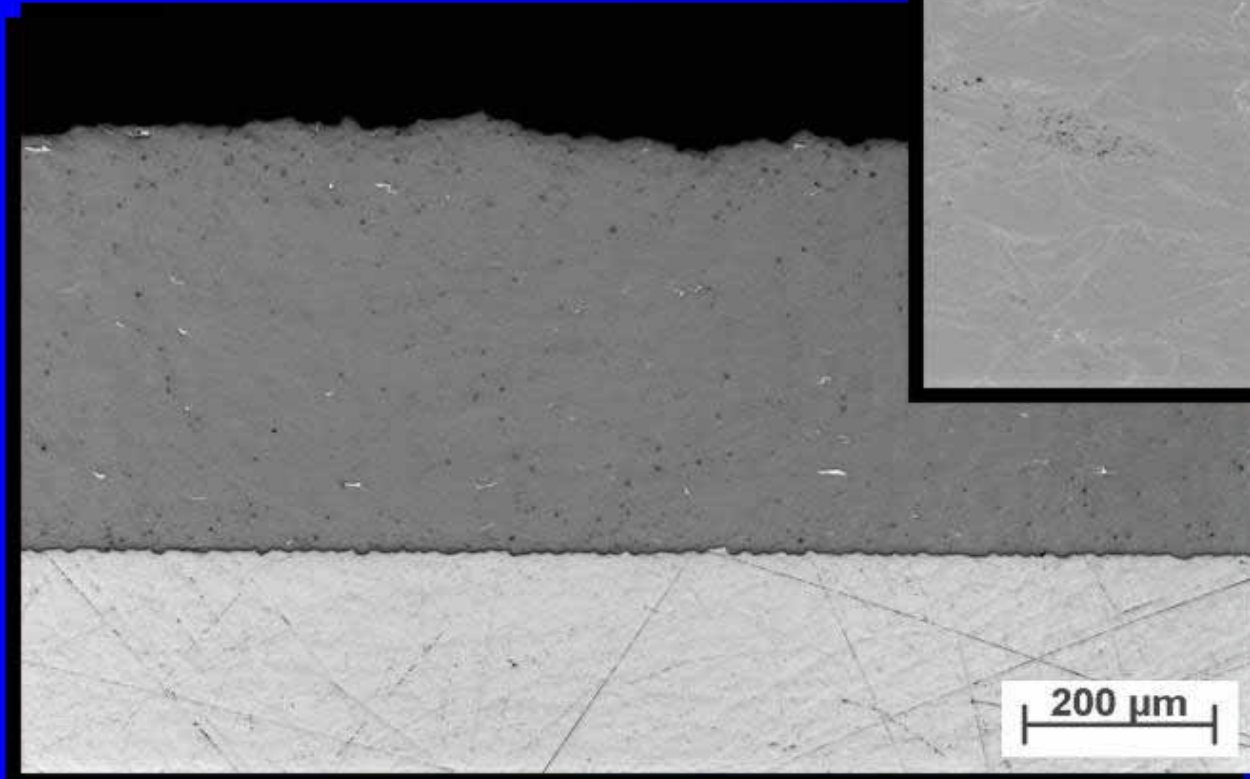
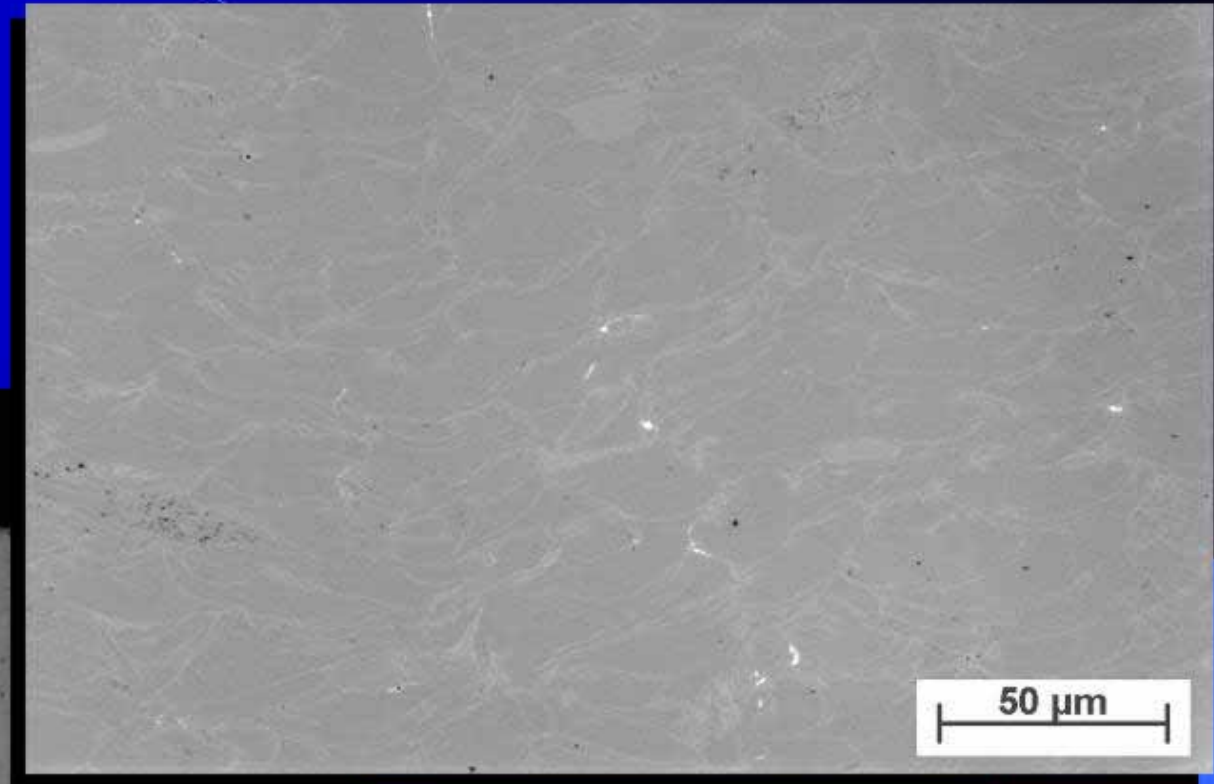


etched



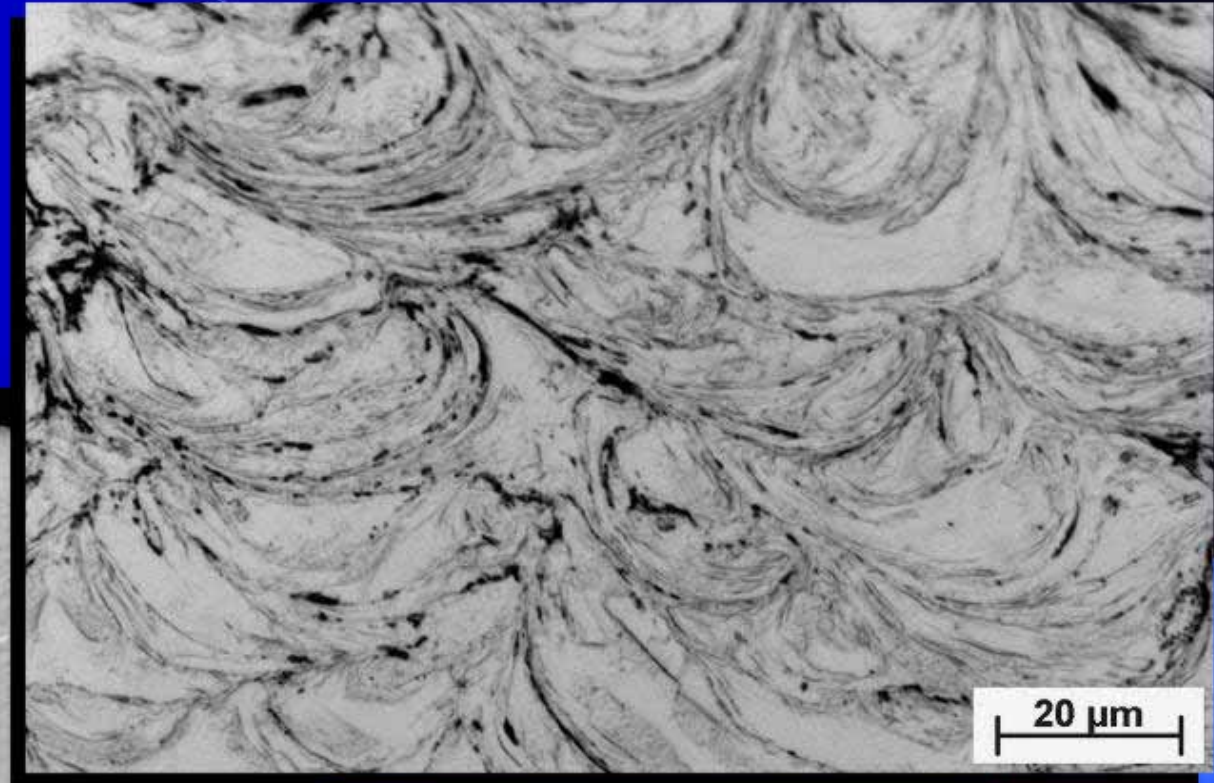
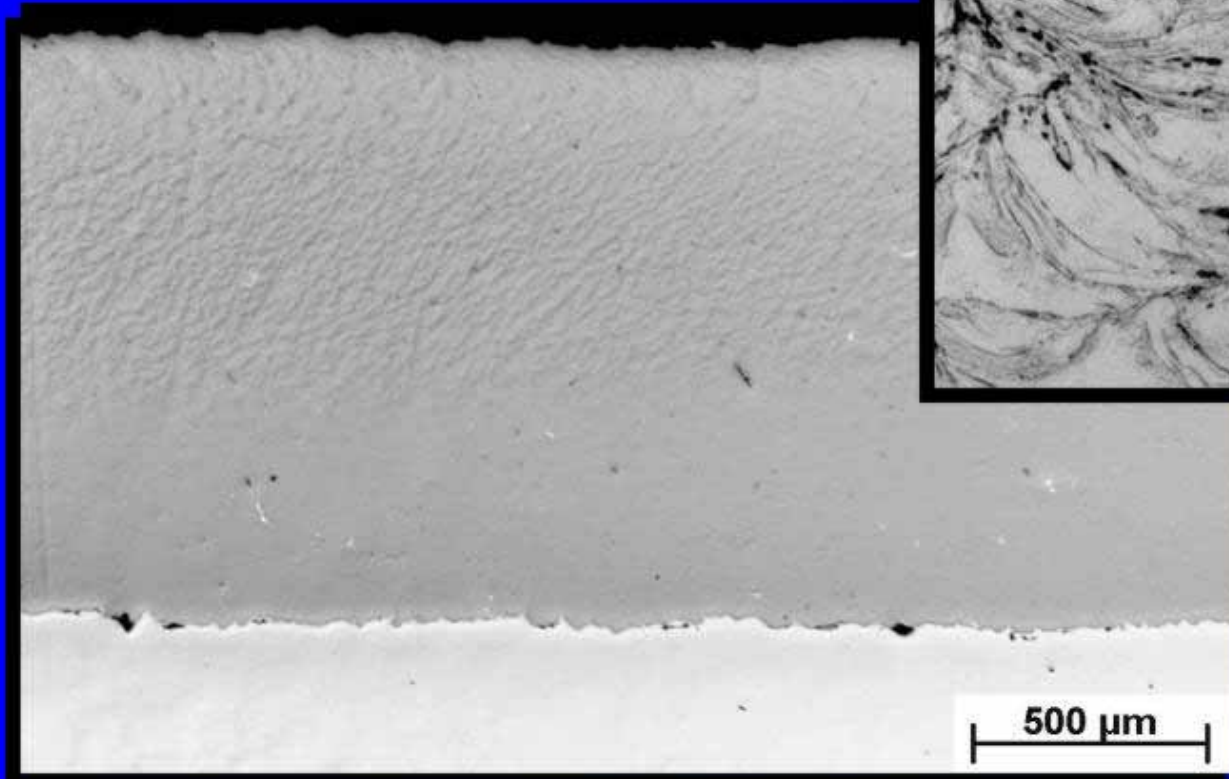
Ta Coating (N₂)

TCT-test: 210 MPa



Ta Coating (He)

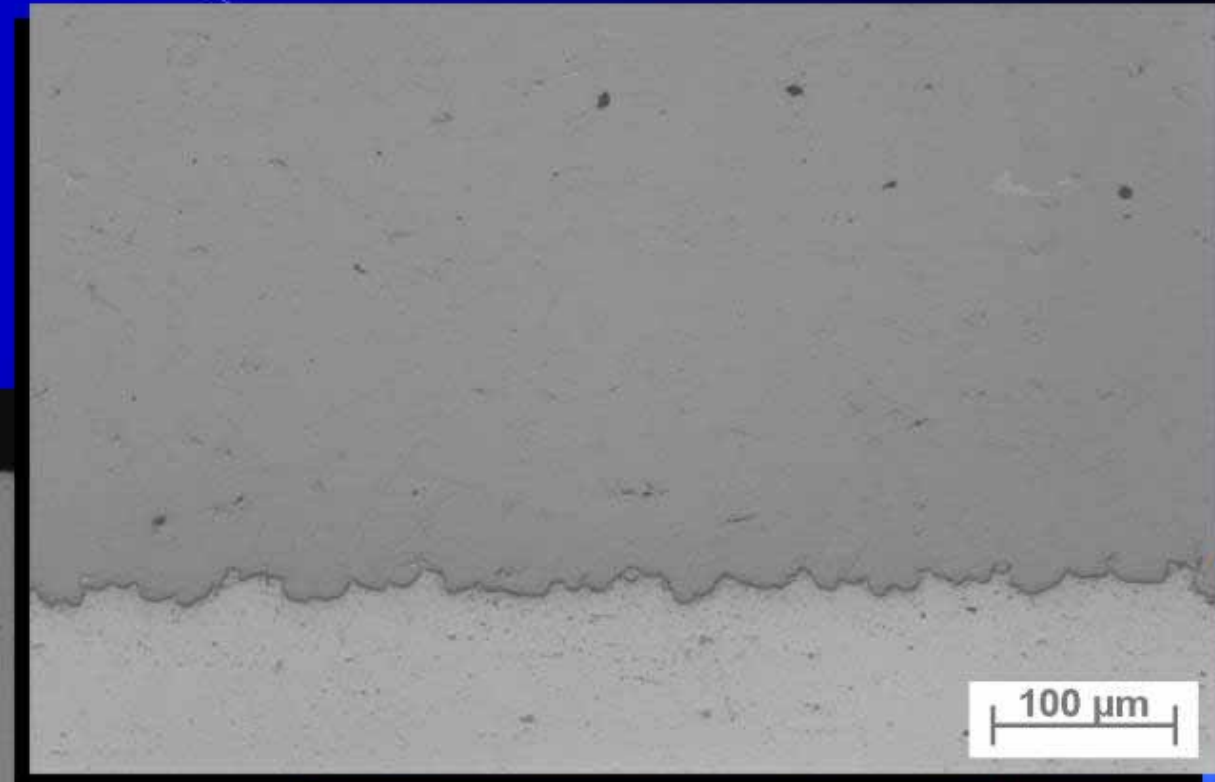
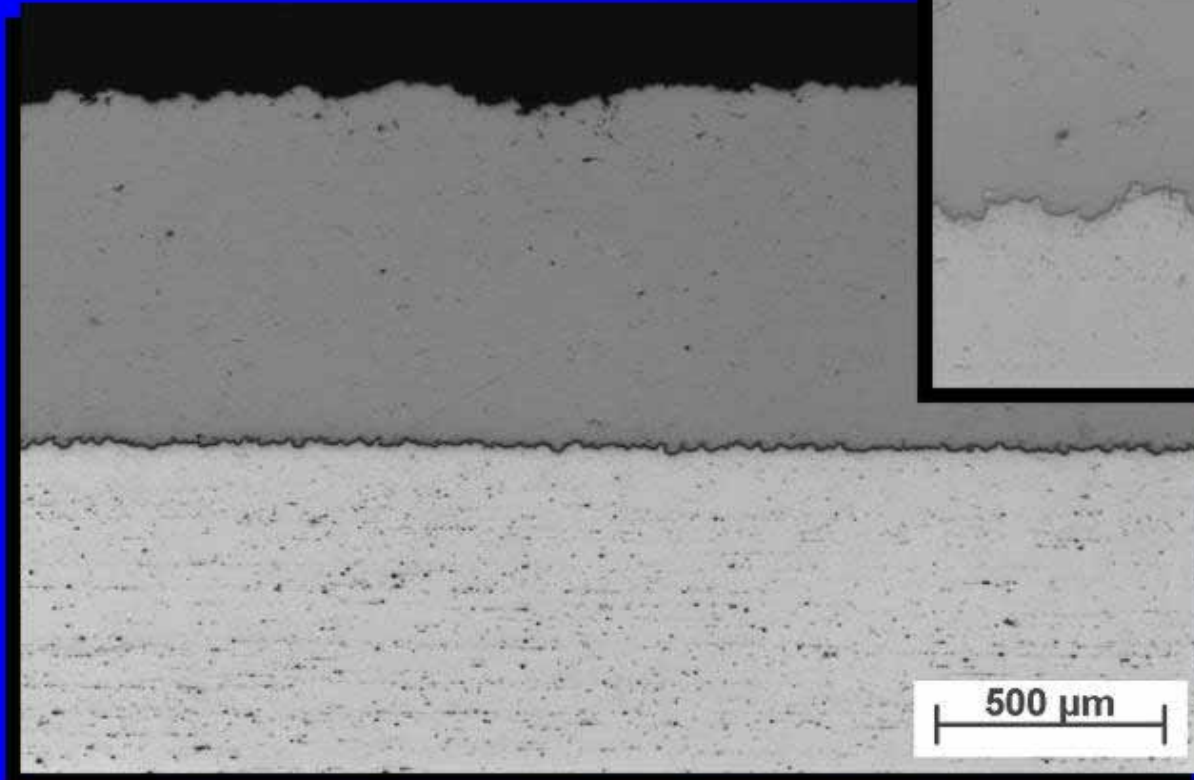
TCT-test: 290 MPa



etched

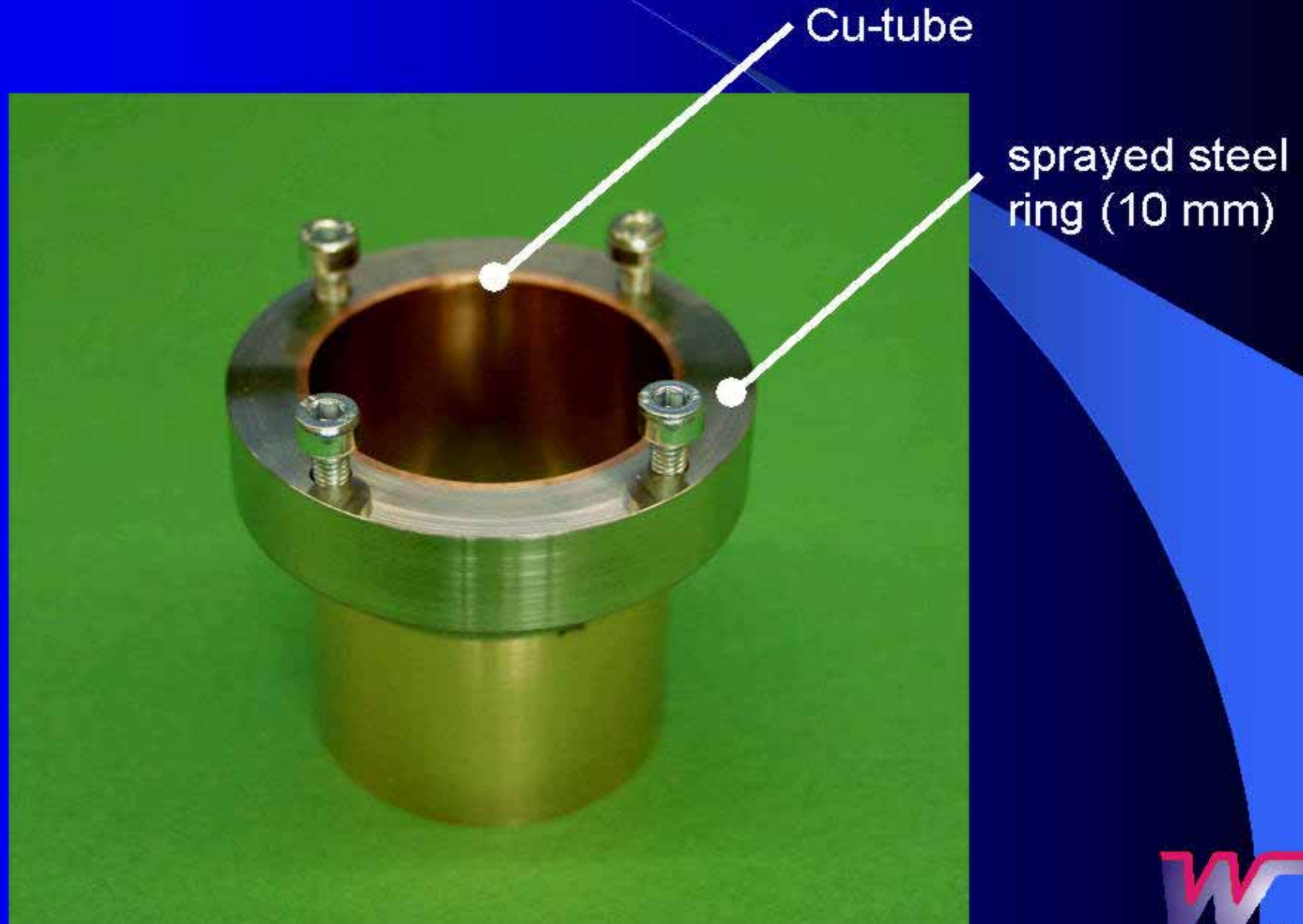
Steel 316L Coating (N₂)

TCT-test: 230 MPa



Spraying of Thick Coatings

repair applications, spray forming, rapid prototyping



Conclusions I

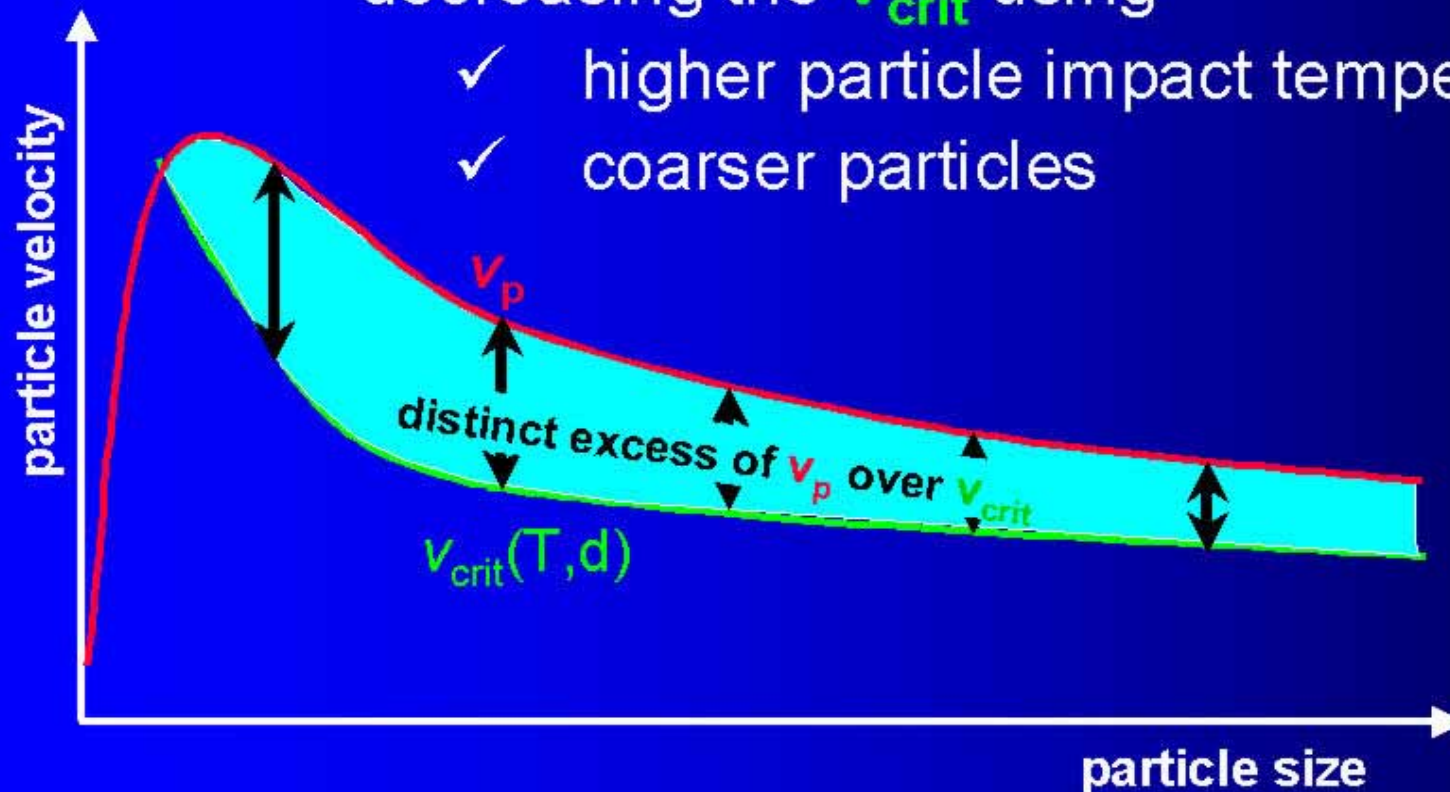
distinct excess of **impact velocity** over **critical velocity** was achieved by:

higher impact velocities using

- ✓ higher gas temperatures and gas pressures
- ✓ optimized nozzle shape and length

decreasing the v_{crit} using

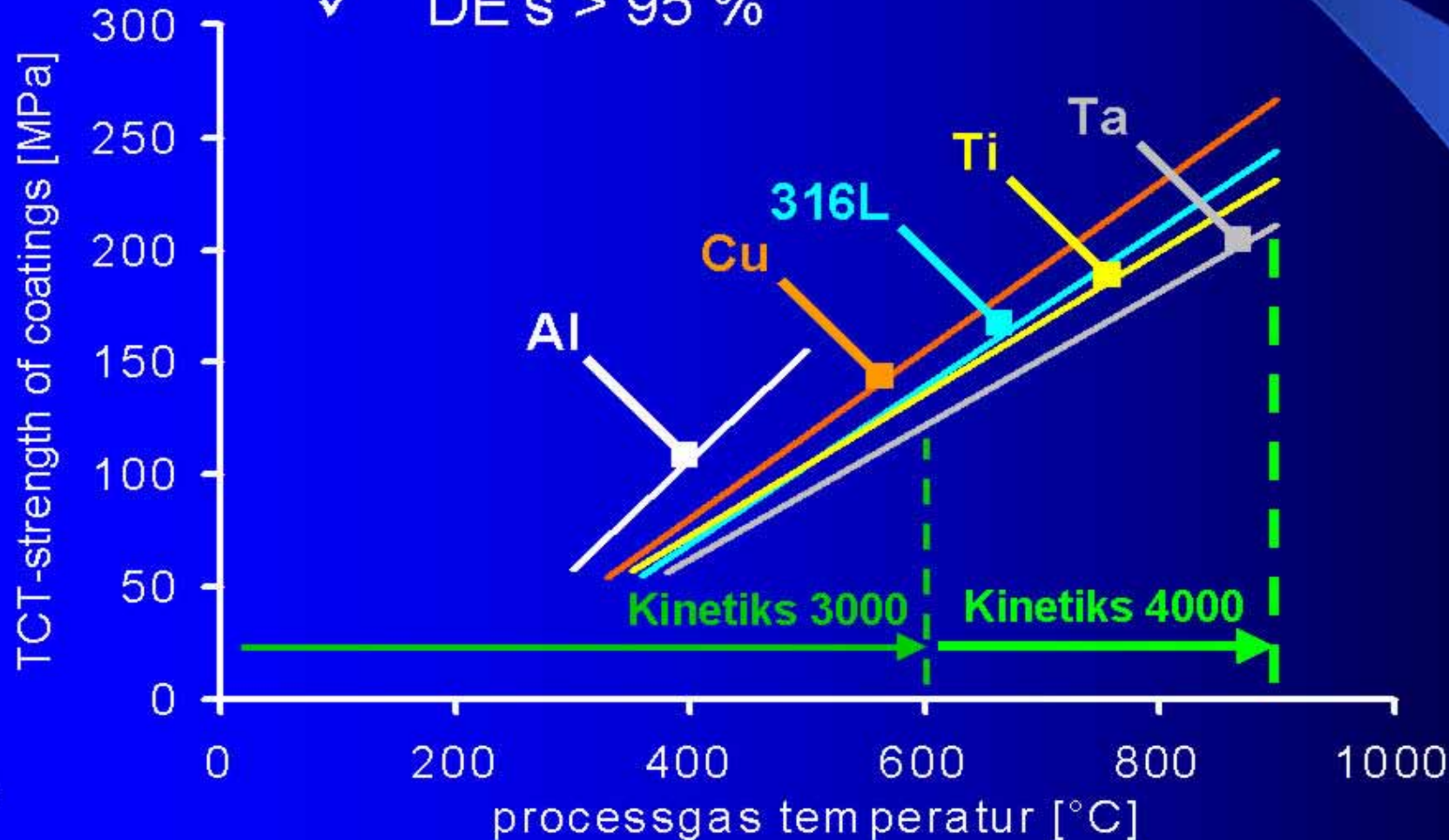
- ✓ higher particle impact temperatures and
- ✓ coarser particles



Conclusions II

The results of these optimization steps are

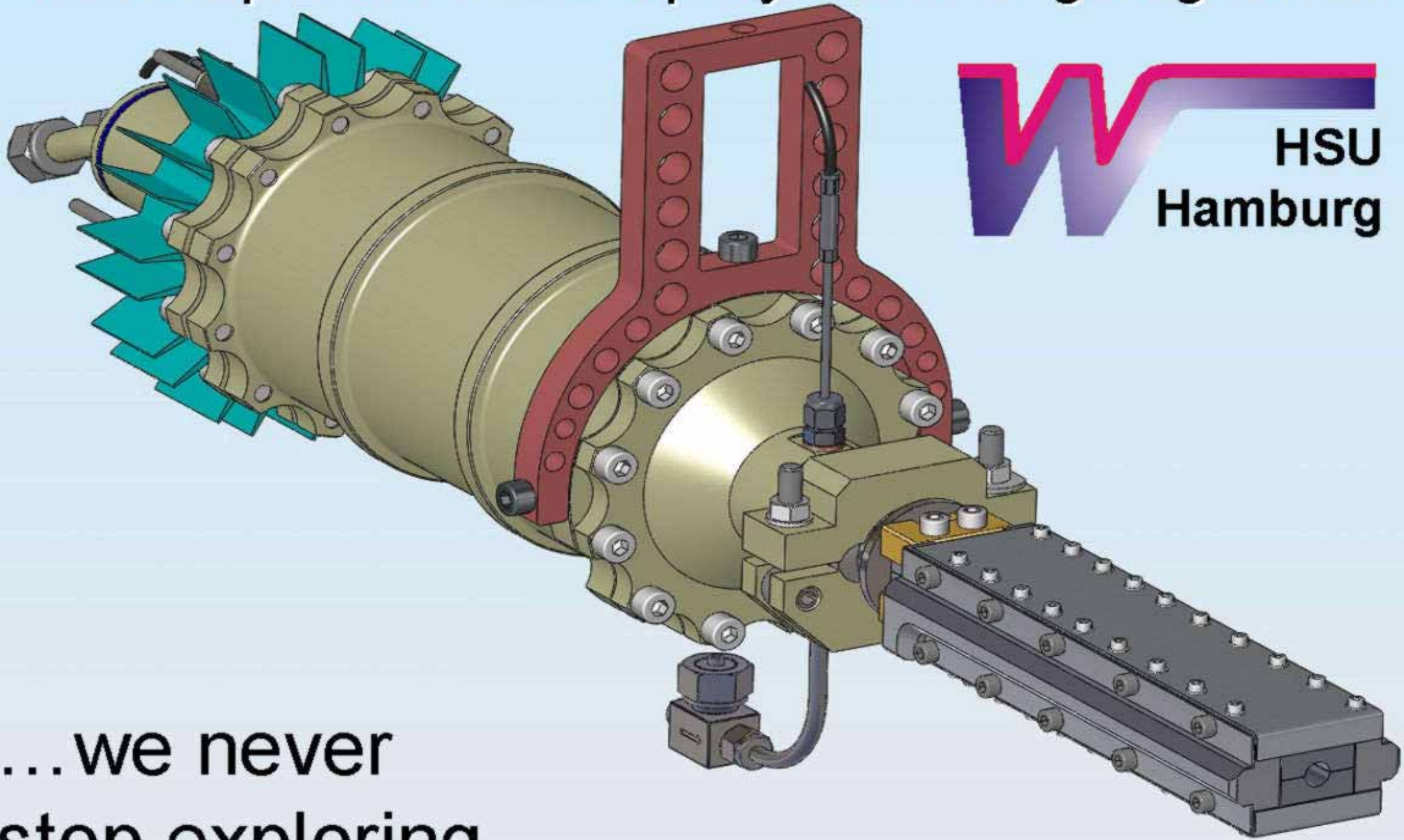
- ✓ extended range of usable spray materials
- ✓ high coating strength
- ✓ dense coatings
- ✓ DE's > 95 %



Literature

- [1] **An Analysis of the Cold Spray Process and its Coatings:** T. Stoltenhoff, H. Kreye, and H.J. Richter, *J. Thermal Spray Technol.*, 11, 2002, p 542-550.
- [2] **Bonding Mechanism in Cold Gas Spraying:** H. Assadi, F. Gärtner, T. Stoltenhoff, and H. Kreye, *Acta Mater.* 51, 2003, p 4379-4394.
- [3] **Development of a Generalized Parameter Window for Cold Spray Deposition:** T. Schmidt, F. Gärtner, H. Assadi, and H. Kreye, *Acta Mater.* 54, 2006, p 729-742.
- [4] **New Developments in Cold Spray Based on Higher Gas- and Particle Temperatures:** T. Schmidt, F. Gärtner, and H. Kreye, *Journal of Thermal Spray Technology*, 15(4), 2006, S. 488-494.
- [5] **Kaltgasspritzen – Eine Analyse des Materialverhaltens beim Partikelaufrall und die daraus abgeleitete Prozessoptimierung:** T. Schmidt, Shaker Verlag, Mai 2007, ISBN 978-3-8322-6399-7.
- [6] **Mechanical Properties of Cold Sprayed and Thermally Sprayed Copper Coatings:** F. Gärtner, T. Stoltenhoff, J. Voyer, and H. Kreye, *Surf. Coat. Techno.* 200, 2006, p 6770-6782.

Development of CS Spray Guns is going on at



...we never
stop exploring.

Collaboration

Cold Spray Competence Group



H.J. Richter

fluid dynamics

mechanisms, materials, equipment



T. Klassen, H. Kreye

materials science



P. Heinrich

gas technology

gas supply



P. Richter

spray systems

equipment, license



A. Eiling

spray materials

spray powder

evaluation of applications

support to industry