

LEIS BÁSICAS DA TRANSFERÊNCIA DE CALOR

Lei de Fourier: $q = -k A \frac{\partial T}{\partial x}$

Lei de Newton do resfriamento: $q = h A (T_s - T_\infty)$

Lei de Stefan-Boltzmann:

$$q = \sigma \varepsilon_1 A_1 (T_1^4 - T_2^4); \quad \sigma = 5,6697 \times 10^{-8} \text{ W/m}^2 \text{K}^4$$

Analogia entre convecção e radiação: $h_{rad} = \sigma \varepsilon_1 (T_1^2 + T_2^2) (T_1 + T_2)$

Energia gerada: $q_{ger} = \dot{q} V$

Energia acumulada: $q = m c_p \frac{\partial T}{\partial t} = \rho V c_p \frac{\partial T}{\partial t} = \dot{m} c_p \Delta T = \dot{m} h_v$

EQUAÇÃO DA DIFUSÃO DE CALOR

COORDENADAS CARTESIANAS

$$\frac{\partial}{\partial x} \left(k \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left(k \frac{\partial T}{\partial y} \right) + \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

COORDENADAS CILÍNDRICAS

$$\frac{1}{r} \frac{\partial}{\partial r} \left(k r \frac{\partial T}{\partial r} \right) + \frac{1}{r^2} \frac{\partial}{\partial \phi} \left(k \frac{\partial T}{\partial \phi} \right) + \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

COORDENADAS ESFÉRICAS

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(k r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \phi} \left(k \frac{\partial T}{\partial \phi} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(k \sin \theta \frac{\partial T}{\partial \theta} \right) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

ANALOGIA ENTRE CIRCUITOS ELÉTRICOS E TÉRMICOS

Taxa de transferência de calor: $q = \frac{\Delta T}{R_t}$

Parede plana (condução): $R_t = \frac{L}{k A}$

Parede cilíndrica (condução): $R_t = \frac{\ln(r_e / r_i)}{2 \pi k L}$

Parede esférica (condução): $R_t = \frac{1}{4 \pi k} \left(\frac{1}{r_1} - \frac{1}{r_2} \right)$

Convecção: $R_t = \frac{1}{h A}$

SUPERFÍCIES ESTENDIDAS (ALETAS)

Excesso de temperatura: $\theta(x) = T(x) - T_\infty$

$$m^2 = \frac{h P}{k A_{tr}}$$

sendo: h o coeficiente convectivo, P o perímetro da aleta, k a condutividade térmica e A_{tr} a área da seção transversal da aleta.

Efetividade da aleta: $\varepsilon_a = \frac{q_a}{h A_{tr,b} \theta_b}$

sendo $A_{tr,b}$ a área da seção transversal da aleta em sua base.

Eficiência da aleta: $\eta = \frac{q_a}{q_{max}} = \frac{q_a}{h A_a \theta_b}$

sendo A_a a área superficial da aleta.

TABELA 3.5 Eficiência de aletas com formas comuns

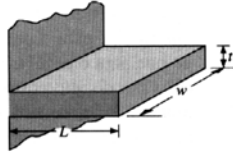
Aletas Planas

Retangular^a

$$A_a = 2wL_c$$

$$L_c = L + (t/2)$$

$$A_p = tL$$

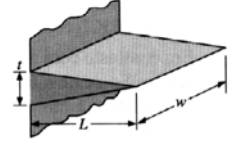


$$\eta_a = \frac{\tanh mL_c}{mL_c}$$

Triangular^a

$$A_a = 2w[L^2 + (t/2)^2]^{1/2}$$

$$A_p = (t/2)L$$



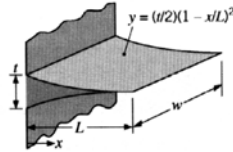
$$\eta_a = \frac{1}{mL} \frac{I_1(2mL)}{I_0(2mL)}$$

Parabólica^a

$$A_a = w[C_1L + (L^2/t)\ln(tL + C_1)]$$

$$C_1 = [1 + (tL)^2]^{1/2}$$

$$A_p = (t/3)L$$



$$\eta_a = \frac{2}{[4(mL)^2 + 1]^{1/2} + 1}$$

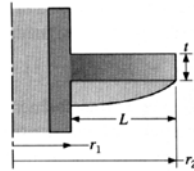
Aleta Circular

Retangular^a

$$A_a = 2\pi(r_{2c}^2 - r_1^2)$$

$$r_{2c} = r_2 + (t/2)$$

$$V = \pi(r_2^2 - r_1^2)t$$



$$\eta_a = C_2 \frac{K_1(mr_1)I_1(mr_{2c}) - I_1(mr_1)K_1(mr_{2c})}{I_0(mr_1)K_1(mr_{2c}) + K_0(mr_1)I_1(mr_{2c})}$$

$$C_2 = \frac{(2r_1/m)}{(r_{2c}^2 - r_1^2)}$$

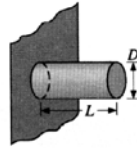
Aletas em Forma de Pino

Retangular^b

$$A_a = \pi DL_c$$

$$L_c = L + (D/4)$$

$$V = (\pi D^2/4)L$$

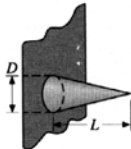


$$\eta_a = \frac{\tanh mL_c}{mL_c}$$

Triangular^b

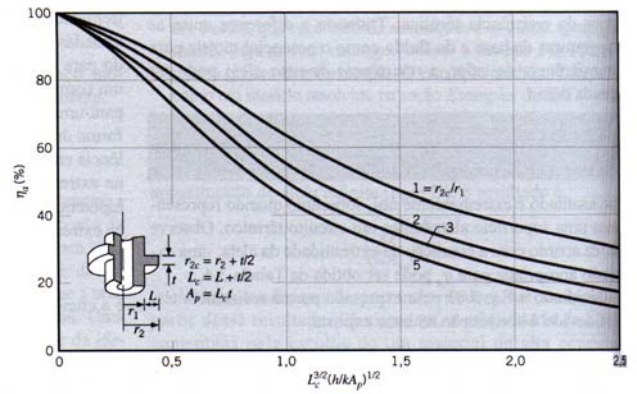
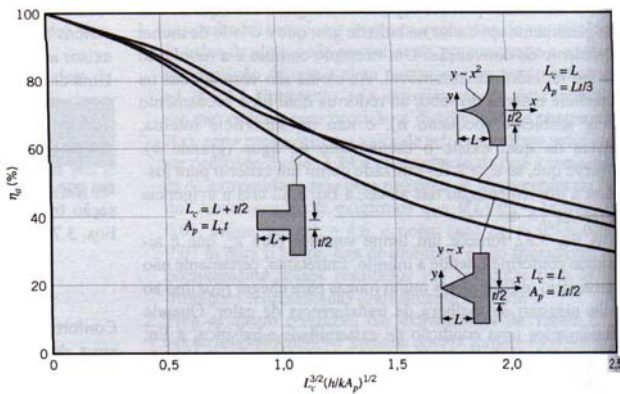
$$A_a = \frac{\pi D}{2} [L^2 + (D/2)^2]^{1/2}$$

$$V = (\pi/12)D^2L$$



$$\eta_a = \frac{2}{mL} \frac{I_2(2mL)}{I_1(2mL)}$$

^a $m = (2h/kt)^{1/2}$
^b $m = (4h/kD)^{1/2}$



B.5 Funções¹ de Bessel Modificadas de Primeira e Segunda Espécies

| x | $e^{-x}I_0(x)$ | $e^{-x}I_1(x)$ | $e^xK_0(x)$ | $e^xK_1(x)$ |
|------|----------------|----------------|-------------|-------------|
| 0,0 | 1,0000 | 0,0000 | ∞ | ∞ |
| 0,2 | 0,8269 | 0,0823 | 2,1407 | 5,8334 |
| 0,4 | 0,6974 | 0,1368 | 1,6627 | 3,2587 |
| 0,6 | 0,5993 | 0,1722 | 1,4167 | 2,3739 |
| 0,8 | 0,5241 | 0,1945 | 1,2582 | 1,9179 |
| 1,0 | 0,4657 | 0,2079 | 1,1445 | 1,6361 |
| 1,2 | 0,4198 | 0,2152 | 1,0575 | 1,4429 |
| 1,4 | 0,3831 | 0,2185 | 0,9881 | 1,3010 |
| 1,6 | 0,3533 | 0,2190 | 0,9309 | 1,1919 |
| 1,8 | 0,3289 | 0,2177 | 0,8828 | 1,1048 |
| 2,0 | 0,3085 | 0,2153 | 0,8416 | 1,0335 |
| 2,2 | 0,2913 | 0,2121 | 0,8056 | 0,9738 |
| 2,4 | 0,2766 | 0,2085 | 0,7740 | 0,9229 |
| 2,6 | 0,2639 | 0,2046 | 0,7459 | 0,8790 |
| 2,8 | 0,2528 | 0,2007 | 0,7206 | 0,8405 |
| 3,0 | 0,2430 | 0,1968 | 0,6978 | 0,8066 |
| 3,2 | 0,2343 | 0,1930 | 0,6770 | 0,7763 |
| 3,4 | 0,2264 | 0,1892 | 0,6579 | 0,7491 |
| 3,6 | 0,2193 | 0,1856 | 0,6404 | 0,7245 |
| 3,8 | 0,2129 | 0,1821 | 0,6243 | 0,7021 |
| 4,0 | 0,2070 | 0,1787 | 0,6093 | 0,6816 |
| 4,2 | 0,2016 | 0,1755 | 0,5953 | 0,6627 |
| 4,4 | 0,1966 | 0,1724 | 0,5823 | 0,6453 |
| 4,6 | 0,1919 | 0,1695 | 0,5701 | 0,6292 |
| 4,8 | 0,1876 | 0,1667 | 0,5586 | 0,6142 |
| 5,0 | 0,1835 | 0,1640 | 0,5478 | 0,6003 |
| 5,2 | 0,1797 | 0,1614 | 0,5376 | 0,5872 |
| 5,4 | 0,1762 | 0,1589 | 0,5279 | 0,5749 |
| 5,6 | 0,1728 | 0,1565 | 0,5188 | 0,5633 |
| 5,8 | 0,1696 | 0,1542 | 0,5101 | 0,5525 |
| 6,0 | 0,1666 | 0,1520 | 0,5019 | 0,5422 |
| 6,4 | 0,1611 | 0,1479 | 0,4865 | 0,5232 |
| 6,8 | 0,1561 | 0,1441 | 0,4724 | 0,5060 |
| 7,2 | 0,1515 | 0,1405 | 0,4595 | 0,4905 |
| 7,6 | 0,1473 | 0,1372 | 0,4476 | 0,4762 |
| 8,0 | 0,1434 | 0,1341 | 0,4366 | 0,4631 |
| 8,4 | 0,1398 | 0,1312 | 0,4264 | 0,4511 |
| 8,8 | 0,1365 | 0,1285 | 0,4168 | 0,4399 |
| 9,2 | 0,1334 | 0,1260 | 0,4079 | 0,4295 |
| 9,6 | 0,1305 | 0,1235 | 0,3995 | 0,4198 |
| 10,0 | 0,1278 | 0,1213 | 0,3916 | 0,4108 |

$${}^1I_{n+1}(x) = I_{n-1}(x) - (2n/x)I_n(x)$$