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SURFACE DURABILITY OF WORM GEAR

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This information is applicable for worm gear pair drives that are used to transmit power in general industrial machines with the following parameters:

Axial module / m_a / 1 – 25mm

Pitch diameter of worm wheel / d_2 / 900mm or less

Sliding speed / v_s / 30m/s or less

Rotational speed of worm wheel / n_2 / 600rpm or less

(1)Basic Formulas

(1)-1 Sliding speed (m/s)

$$v_s = \frac{d_{01} n_1}{19100 \cos \gamma_0} \quad (10.51)$$

(1)-2 Torque, tangential force and efficiency

1. Worm as driver (Speed reducing)



BEVEL GEARBOX

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$$\begin{aligned}
 T_2 &= \frac{F_t d_{02}}{2000} \\
 T_1 &= \frac{T_2}{i \eta_R} = \frac{F_t d_{02}}{2000 i \eta_R} \\
 \eta_R &= \frac{\tan \gamma_0 \left(1 - \tan \gamma_0 \frac{\mu}{\cos \alpha_n} \right)}{\tan \gamma_0 + \frac{\mu}{\cos \alpha_n}}
 \end{aligned}
 \quad \left. \vphantom{\begin{aligned} T_2 \\ T_1 \\ \eta_R \end{aligned}} \right\} (10.52)$$

Where

T_2 : Nominal torque of worm wheel (kgf · m)

T_1 : Nominal torque of worm (kgf · m)

F_t : Nominal tangential force on worm wheel's pitch circle (kgf)

d_{02} : Pitch diameter of worm wheel (mm)

i : Gear ratio = z_2 / z_w

η_R : Transmission efficiency, worm driving (not including bearing loss, lubricant agitation loss, etc.)

μ : Coefficient of friction

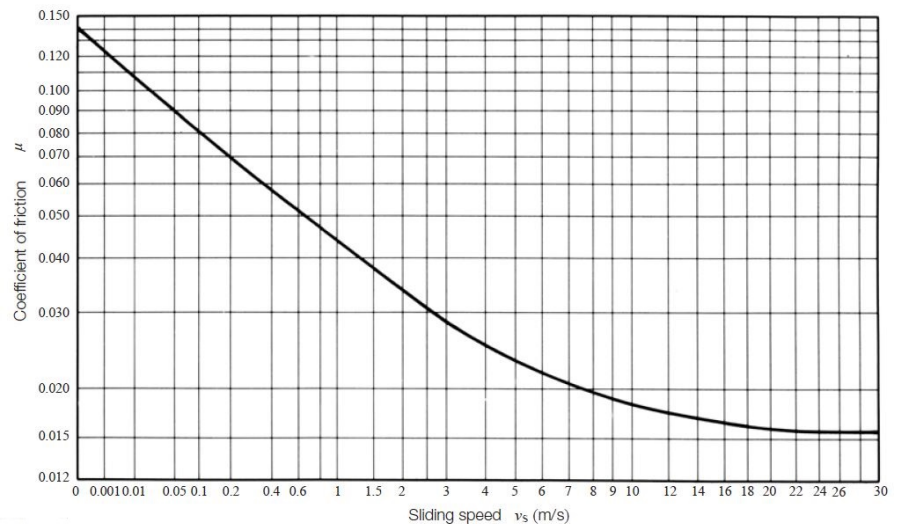
2. Worm wheel as driver (Speed increasing)

$$\begin{aligned}
 T_2 &= \frac{F_t d_{02}}{2000} \\
 T_1 &= \frac{T_2 \eta_I}{i} = \frac{F_t d_{02} \eta_I}{2000 i} \\
 \eta_I &= \frac{\tan \gamma_0 - \frac{\mu}{\cos \alpha_n}}{\tan \gamma_0 \left(1 + \tan \gamma_0 \frac{\mu}{\cos \alpha_n} \right)}
 \end{aligned}
 \quad \left. \vphantom{\begin{aligned} T_2 \\ T_1 \\ \eta_I \end{aligned}} \right\} (10.53)$$

Where η_I : Transmission efficiency, worm wheel driving (not including bearing loss, lubricant agitation loss, etc.)



Fig. 10.12 Coefficient of Friction



For lack of data, coefficient of friction, μ , of materials is very difficult to obtain.

However, Table 10.27 indicates H. E. Merritt's offer as a reference.

Table 10.27 Combination of materials and their coefficients of friction, μ

Combination of materials	Values of μ
Cast iron and phosphor bronze	μ in Figure 10.12 times 1.15
Cast iron and cast iron	μ in Figure 10.12 times 1.33
Quenched steel and aluminum alloy	μ in Figure 10.12 times 1.33
Steel and steel	μ in Figure 10.12 times 2.00

3. Coefficient of friction, μ

The coefficient of friction, μ , varies as sliding speed, v_s , changes. The combination of materials is important. For the case of a worm that is carburized and ground, and mated with a phosphorous bronze worm wheel, see Figure 10.12.

(2) Calculation of Allowable Load to Surface Durability

(2)-1 Calculation of Basic Load

Provided dimensions and materials of the worm gear pair are known, the allowable load is as follows:

Allowable tangential force F_{tlim} (kgf)

$$F_{tlim} = 3.82K_v K_n S_{clim} Z d_{02}^{0.8} m_a \frac{Z_L Z_M Z_R}{K_C} \quad (10.54)$$

Allowable worm wheel torque, T_{2lim} (kgf·m)

$$T_{2lim} = 0.00191K_v K_n S_{clim} Z d_{02}^{1.8} m_a \frac{Z_L Z_M Z_R}{K_C} \quad (10.55)$$

(2)-2 Calculation of Equivalent Load

Please note that in such cases, where the starting torque is not more than 200% of the rated torque (NOTE 1) and the frequency of starting is less than twice per hour, are regarded as 'no impact'. In all other cases, the equivalent load is to be calculated and compared to the basic load.

Equivalent load is then converted to an equivalent tangential force, F_{te} (kgf)

$$F_{te} = F_t K_h K_s \quad (10.56)$$

and equivalent worm wheel torque, T_{2e} (kgf · m)

$$T_{2e} = T_2 K_h K_s \quad (10.57)$$

[NOTE 1]

Rated torque denotes the torque on the worm wheel when the motor (or loader) is operating at rated load.

(2)-3 Determination of Load

1. Under no impact condition, to have life expectancy of 26,000 hours, the following relationships must be satisfied:

$$F_t \leq F_{tlim} \text{ or } T_2 \leq T_{2lim} \quad (10.58)$$

2. For all other conditions:

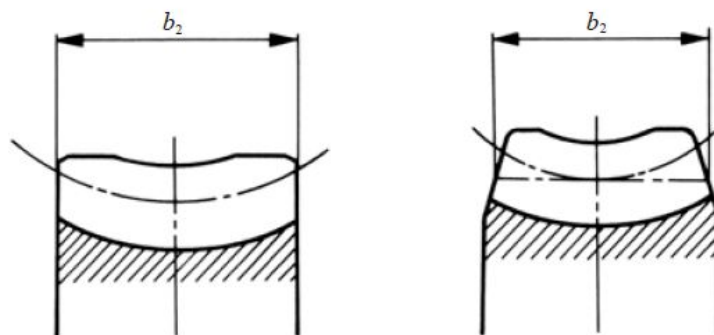
$$F_{te} \leq F_{tlim} \text{ or } T_{2e} \leq T_{2lim} \quad (10.59)$$

NOTE: If load is variable, the comprehensive load, T_{2C} , should be used as the criterion.

(3) Determination of Factors**(3)-1 Facewidth of Worm Wheel, b_2 (mm)**

The facewidth of worm wheel, b_2 , is defined as in Figure 10.13.

Fig. 0.13 Facewidth of worm wheel, b_2

**(3)-2 Zone factor, Z**

$$\left. \begin{array}{l} \textcircled{1} \text{ If } b_2 < 2.3m_a\sqrt{Q+1}, \text{ then} \\ Z = (\text{Basic zone factor}) \times \frac{b_2}{2m_a\sqrt{Q+1}} \\ \textcircled{2} \text{ If } b_2 \geq 2.3m_a\sqrt{Q+1}, \text{ then} \\ Z = (\text{Basic zone factor}) \times 1.15 \end{array} \right\} (10.60)$$

Table 10.28 Basic zone factors

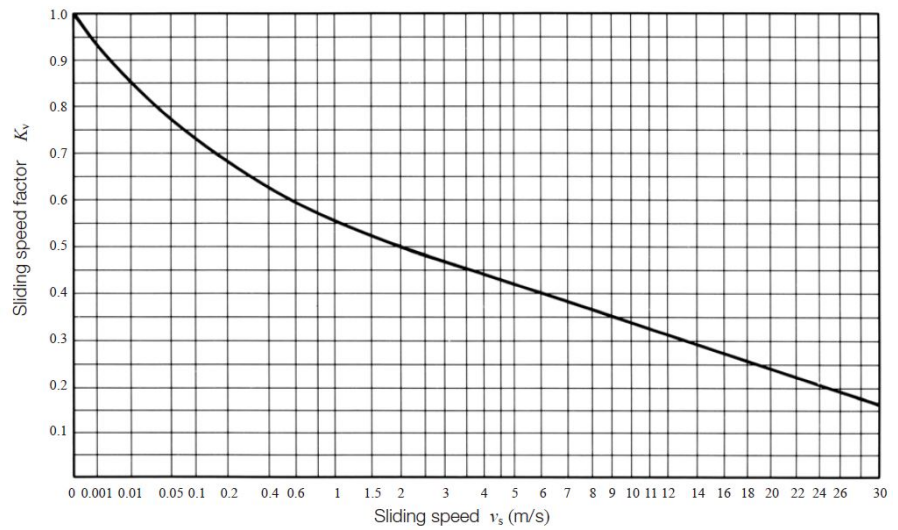
$z_w \backslash Q$	7	7.5	8	8.5	9	9.5	10	11	12	13	14	17	20
1	1.052	1.065	1.084	1.107	1.128	1.137	1.143	1.160	1.202	1.260	1.318	1.402	1.508
2	1.055	1.099	1.144	1.183	1.214	1.223	1.231	1.250	1.280	1.320	1.360	1.447	1.575
3	0.989	1.109	1.209	1.260	1.305	1.333	1.350	1.365	1.393	1.422	1.442	1.532	1.674
4	0.981	1.098	1.204	1.301	1.380	1.428	1.460	1.490	1.515	1.545	1.570	1.666	1.798

Where Q : Diameter factor = $\frac{d_{01}}{m_a}$
 z_w : Number of worm threads

(3)-3 Sliding Speed Factor, K_v

Sliding speed factor, K_v , is obtainable from Figure 10.14, where the abscissa is the sliding speed, v_s .

Fig. 10.14 Sliding speed factor, K_v



(3)-4 Rotational Speed Factor, K_n

The rotational speed factor, K_n , is presented in Figure 10.15 as a function of the worm wheel’s rotational speed, n_2 (rpm).

(3)-5 Lubricant Factor, Z_L

Let $Z_L = 1.0$ if the lubricant is of proper viscosity and has extreme-pressure additives.

Some bearings in worm gearboxes may need a low viscosity lubricant. Then Z_L is to be less than 1.0. The recommended kinetic viscosity of lubrication is given in Table 10.29.



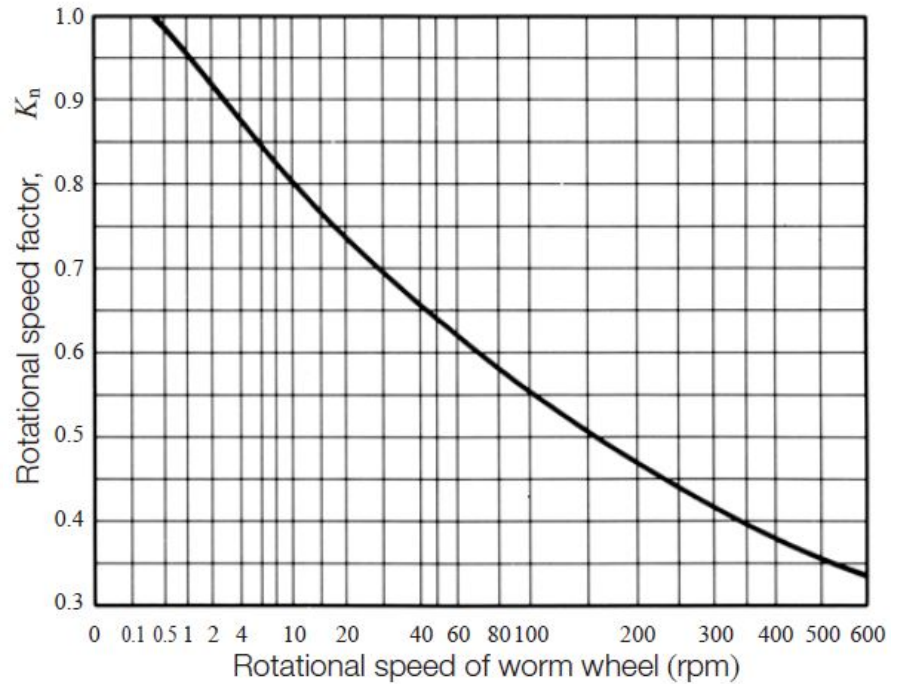
Fig. 10.15 Rotational speed factor, K_n 

Table 10.29 Recommended kinetic viscosity of lubricant

Table 10.29 Recommended kinetic viscosity of lubricant

Unit : cSt/37.8°C

Operating lubricant temperature		Sliding speed m/s		
Highest operating temperature	Lubricant temperature at start of operation	Less than 2.5	2.5 to 5	5 or more
0°C to less than 10°C	-10°C to less 0°C	110 ~ 130	110 ~ 130	110 ~ 130
	More than 0°C	110 ~ 150	110 ~ 150	110 ~ 150
10°C to less than 30°C	More than 0°C	200 ~ 245	150 ~ 200	150 ~ 200
30°C to less than 55°C	More than 0°C	350 ~ 510	245 ~ 350	200 ~ 245
55°C to less than 80°C	More than 0°C	510 ~ 780	350 ~ 510	245 ~ 350
80°C to less than 100°C	More than 0°C	900 ~ 1100	510 ~ 780	350 ~ 510

(3)-6 Lubrication Factor, ZM

The lubrication factor, ZM, is obtained from Table 10.30.

Table 10.30 Lubrication factor, ZM

Sliding speed m/s	Less than 10	10 to 14	14 or more
Oil bath lubrication	1.0	0.85	—
Forced circulation lubrication	1.0	1.0	1.0

(3)-7 Surface Roughness Factor, ZR

The surface roughness factor, ZR, is concerned with resistance to pitting of the working surfaces of the teeth. Since there is insufficient knowledge about this phenomenon, the factor is assumed to be 1.0.

$$Z_R = 1.0 \quad (10.61)$$

It should be noted that for Equation (10.61) to be applicable, surface roughness of the worm and worm wheel must be less than 3S and 12S respectively. If either is rougher, the factor is to be adjusted to a smaller value.

(3)-8 Tooth Contact Factor, KC

Quality of tooth contact will affect load capacity dramatically.

Since it is difficult to prescribe the tooth contact factor, it is usually regarded that K_C for Class A of JIS B 1741 is 1.0.

$K_C = 1.0$ (10.62)

For Class B and C, K_C should be more than 1.0.

Table 1.31 gives the general values of K_C depending on the JIS tooth contact class.

Table 10.31 Classes of tooth contact and general values of tooth contact factor, K_C

Class	Proportion of tooth contact		K_C
	Axial direction	Radial direction	
A	More than 50% of effective length of flank line	More than 40% of working tooth depth	1.0
B	More than 35% of effective length of flank line	More than 30% of working tooth depth	1.3 ~ 1.4
C	More than 20% of effective length of flank line	More than 20% of working tooth depth	1.5 ~ 1.7

(3)-9 Starting Factor, K_S

When starting torque is less than 200% of rated torque, K_S factor is per Table 10.32.

Table 10.32 Starting factor, K_S

(3)-10 Time / Duty Factor, K_h

The time duty factor, K_h , is a function of the desired life and the impact environment. See Table 10.33. The expected lives in between the numbers shown in Table 10.33 can be interpolated.



Table 10.33 Time – duty factor, Kh

NOTE(1) For a machine that operates 10 hours a day, 260 days a year, this number corresponds to ten years of operating life.

(3)-11 Allowable Stress Factor, Sclim

Table 10.34 presents the allowable stress factor, Sclim, for various material combinations. Note that the table also specifies governing limits of sliding speed, which must be adhered to if scoring is to be avoided.

Table 10.34 Allowable stress factor for surface durability, Sclim



NOTE(1) The value indicates the maximum sliding speed within the limit of the allowable stress factor, S_{clim} . Even when the allowable load is below the allowable stress level, if the sliding speed exceeds the indicated limit, there is danger of scoring gear surfaces.

(4) Examples of Calculation



Worm gear pair design details

Surface durability factors and allowable force

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[Strength and Durability of Gears](#) – A page of The ABC's of Gears / Basic Guide – B



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